

X線分析研究懇談会第238回例会：X線検出器

X線検出器の最近の信号処理技術

株式会社テクノエックス
谷口一雄



Photo:ZSX 101

走査型蛍光X線分析装置
ZSXシリーズ

波長分散型

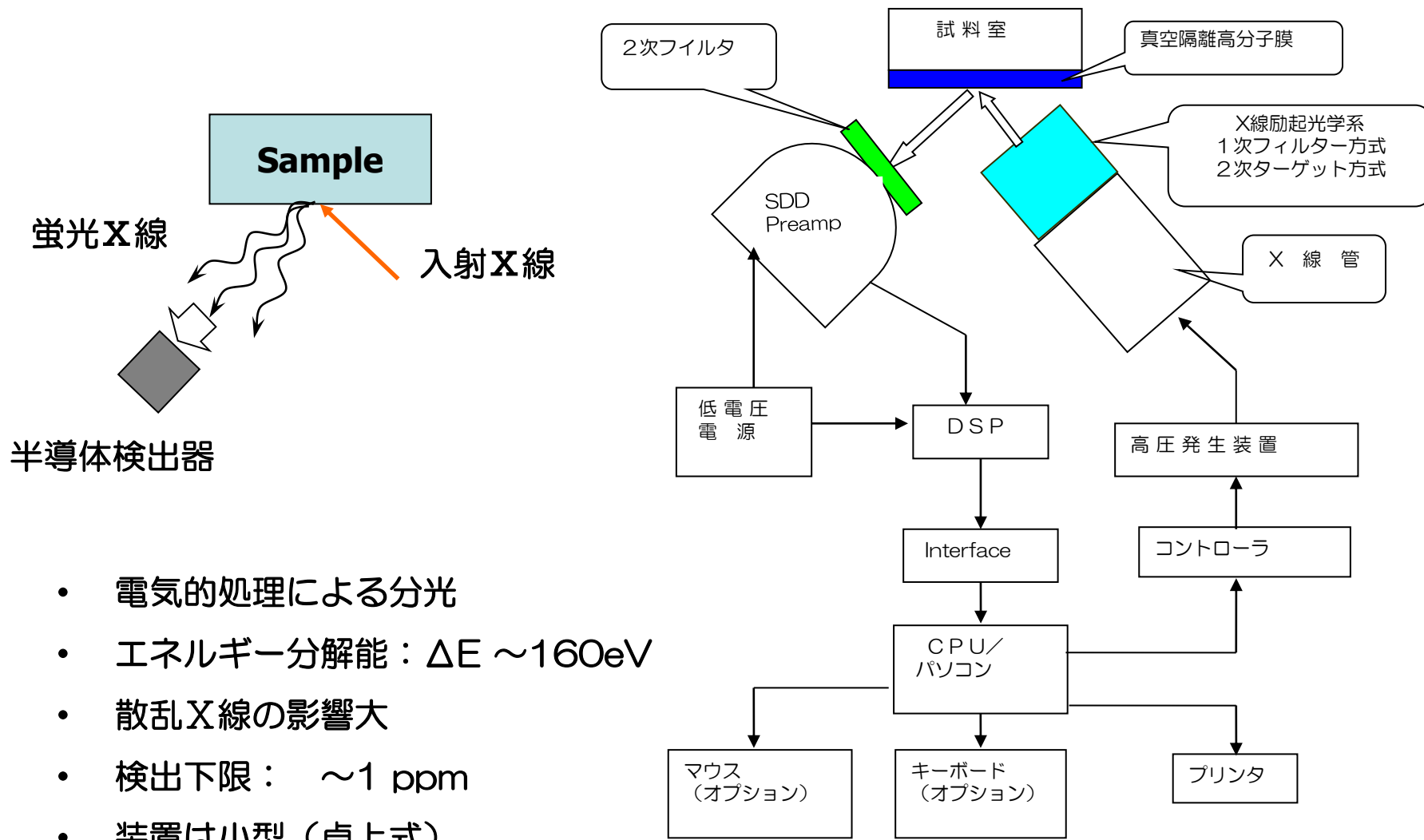
要素技術開発

励起X線源
分光・集光素子
検出器・計測回路



エネルギー分散型

エネルギー分散型蛍光X線分析装置



- 電氣的処理による分光
- エネルギー分解能： $\Delta E \sim 160\text{eV}$
- 散乱X線の影響大
- 検出下限： $\sim 1 \text{ ppm}$
- 装置は小型（卓上式）

励起X線

X線管



小型X線源



検出器

検出素子 (SDD)



小型X線検出器



計測回路



(名刺大)

日 刊 工 業 新 聞

1996年(平成8年)2月8日 木曜日

現場で即座に成分分析

可搬型のX線装置開発

大阪電通大 警備 大庫 兵



大阪電通大学工学部電子
物性工学科の谷口一雄教授は、

兵庫警察科学捜査研究所と共同で「可搬型蛍光X線分析装置」を開発した。犯罪や事故現場に持ち込んで採取したデータを即座に分析、初動段階での捜査、原因究明を迅速に行える。小型で高い分解能を持つX線検出器を半導体で作るための技術開発により実現した。固体と液体を分析でき、洋酒やドル紙幣などの真がんにチェックにも使えるという。持ち運びできるタイプは日本では初めて。

この装置では検出器の半導体素子化に加え、X線発生部も小型化するとともに、0.1〜0.5秒のパルス発振しかできなかったX線発生管を連続発生できるようにして測定プローブ部を構成した。またデータを演算し、解析するコントローラ部はノートパソコンに処理プログラムを搭載、持ち運びを可能にした。

現在、現場で使われている蛍光X線分析装置は、検線がラジオアイソトープのため、移動の際の法的な手続きが煩雑で、海外への持ち出しがとくに難しいという欠点があった。

すでに、谷口教授は事件現場に残されていた検線、検線片などから元素レベルの成分をリアルタイムに分析できる装置を兵庫警察科学捜査研究所と共同で開発している。X線が物質に当たると元素特有の蛍光を発する特性を生かしたもので、そのスペクトルから検線片などの材料も突き止めることができる装置だが、本体寸法が費一枚分ぐらいの大きさで、機動性がなかった。

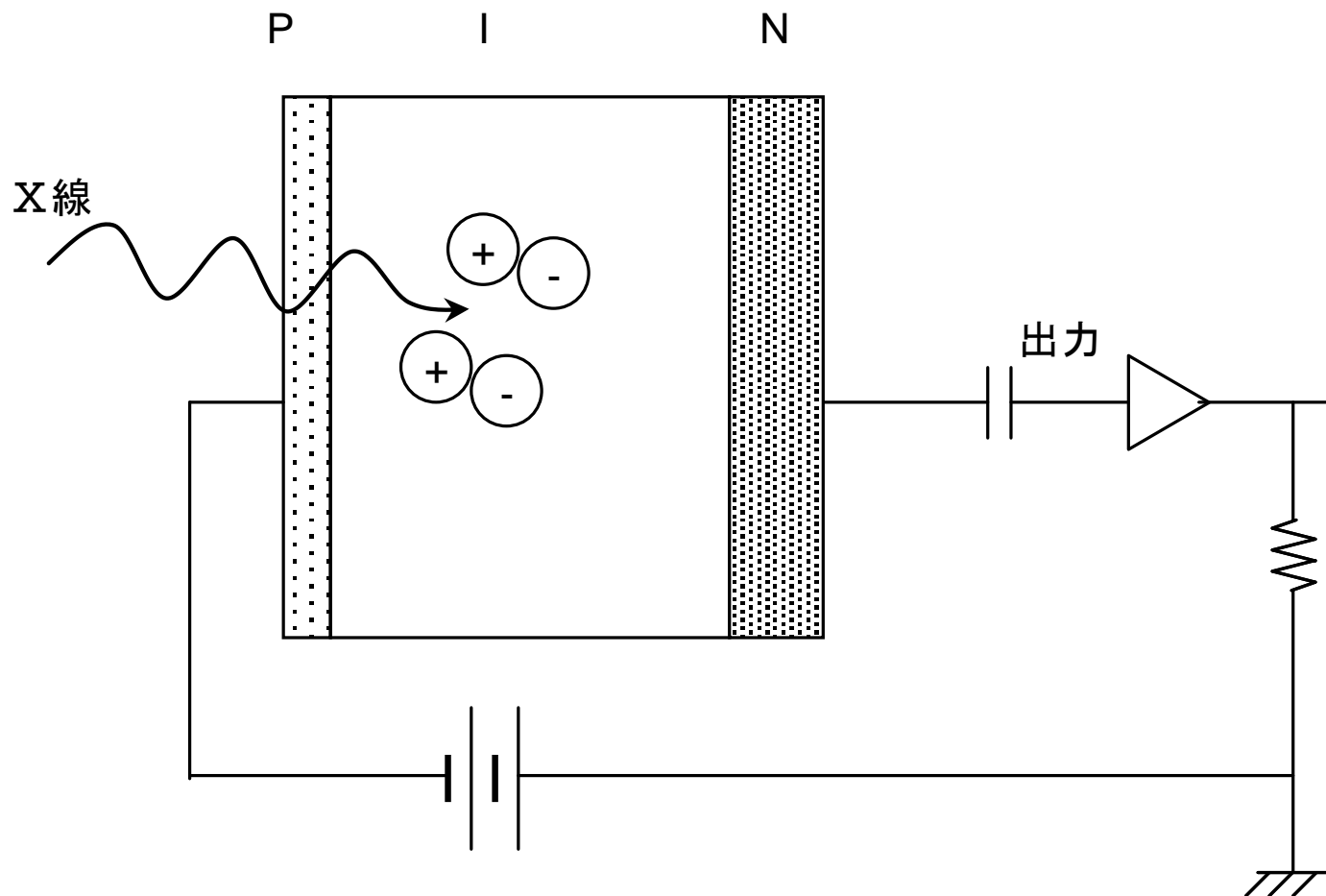
今回の開発により工場排水の取り締まりなども現場でできる道が開けるほか、考古学の発掘調査などの効率化も図れるようになる。

同装置については新技術事業団が企業化開発支援を行うことも決定した。これを受けて谷口教授らは、チタンより軽い金属元素と気体の分析精度や処理速度の向上などをきめた改良を通じて、実用化に取り組む。

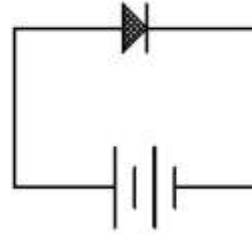


NITON社製

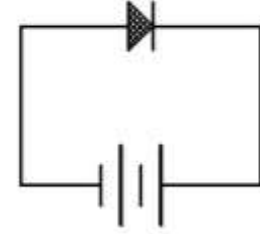




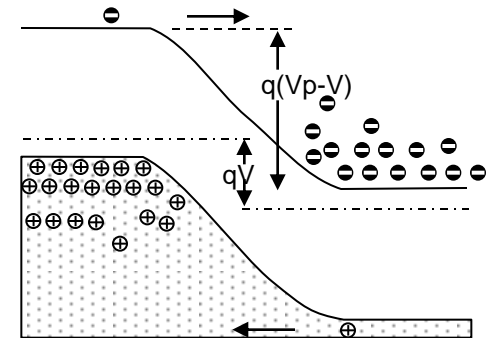
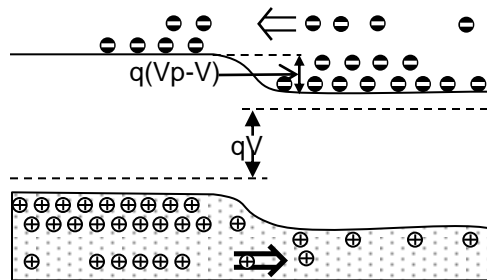
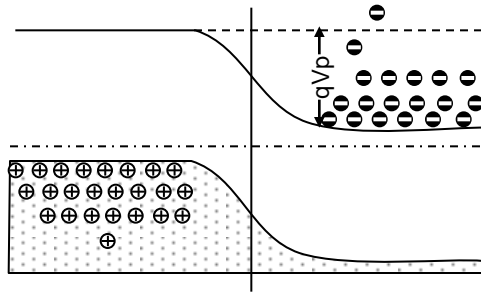
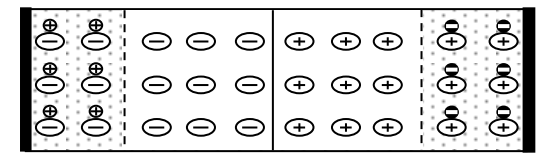
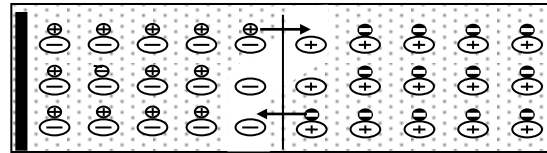
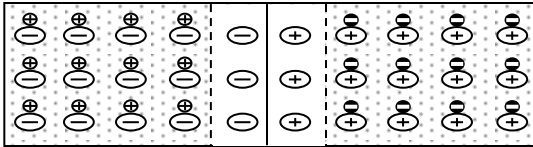
pn-junction as a semiconductor-detector



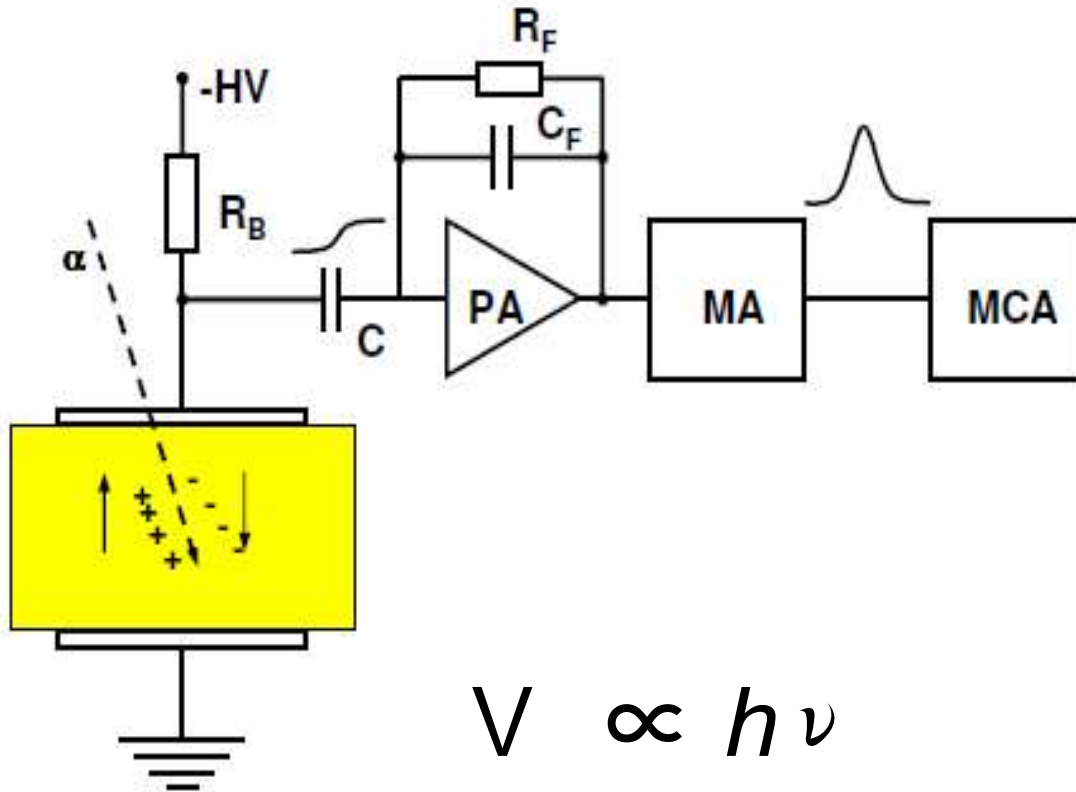
V



V



Principle of solid state detectors



$$N = \frac{h\nu}{\epsilon}$$

E : Energy for e-h pair

N : number of e-h pair

$$Q = eN$$

Q : Charge at input of PA

$$V = \frac{Q}{C} = \frac{eN}{C}$$

V : Voltage at input of P.A

C : capacitance at input of P.A

$$V = \frac{eN}{C} = \frac{eN}{C \cdot \epsilon} \cdot h\nu$$

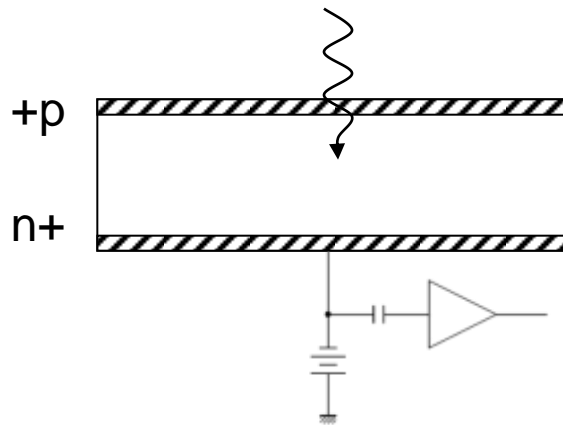
Physical properties of Si, Ge, GaAs, SiC

Properties	Dimension	Si	Ge	GaAs
Atomic number		14	32	31 / 33
Density	g / cm ³	2.33	5.33	5.32
Band gap (RT)	eV	1.12	0.66	1.42
Energy for e-h pair	eV	3.55	2.85	~ 4.1
Electron mobility μ_e	cm ² / V sec	1500	3900	8500
Minority carrier lifetime τ	sec	2.5×10^{-3}	10^{-3}	~ 10^{-8}
Intrinsic resistivity	Ω cm	2.3×10^5	47	10^8

Output $V = \frac{eN}{c}$

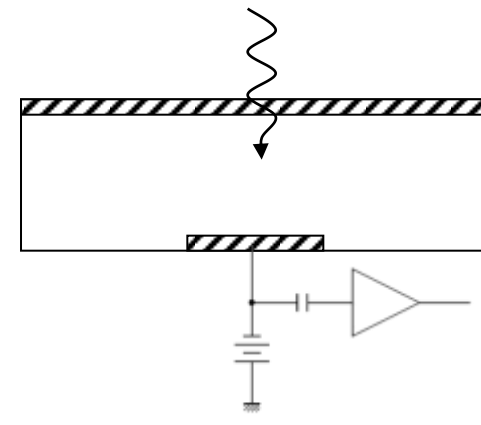
$v \leftarrow$ to large

$c \leftarrow$ to small

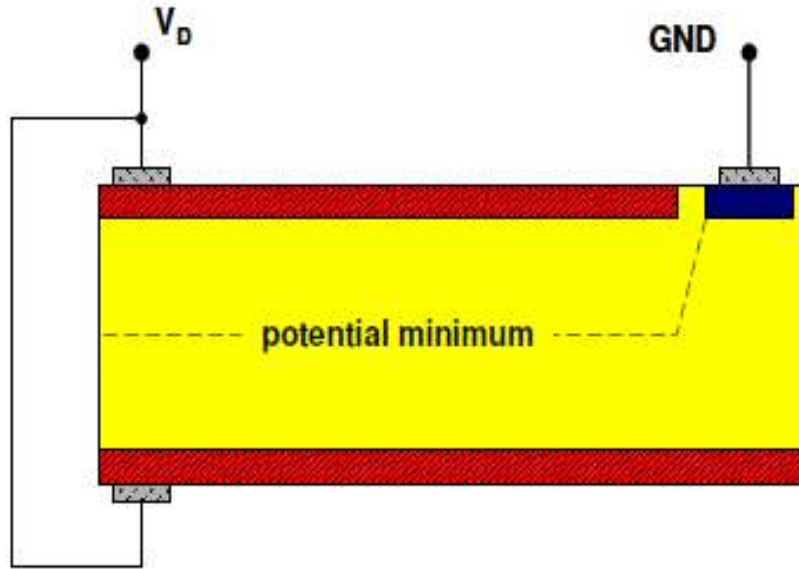


pn- Junction Detector

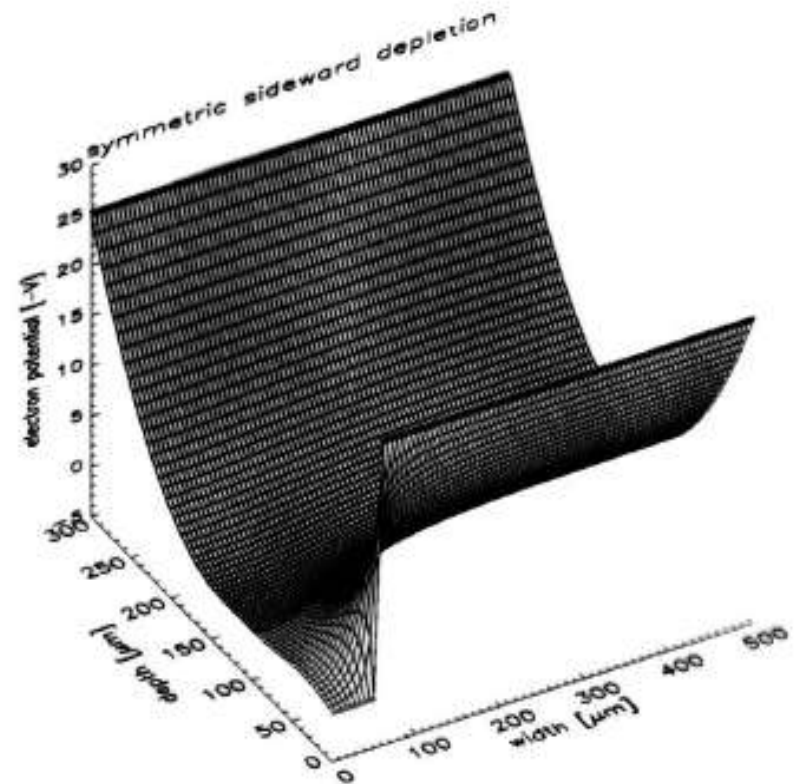
C is reduce



Silicon Drift Detector



Electron potential shows a minimum parallel to the surface

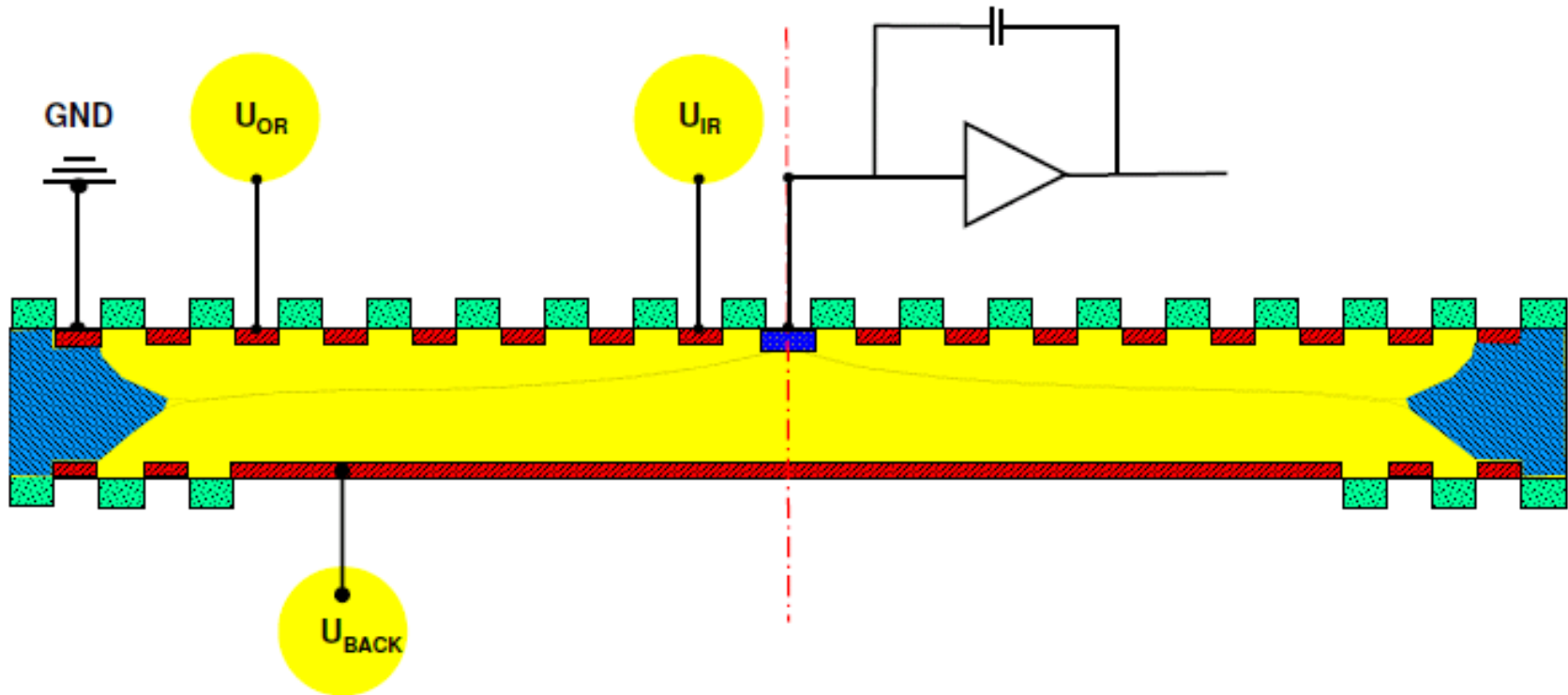


Charge collection

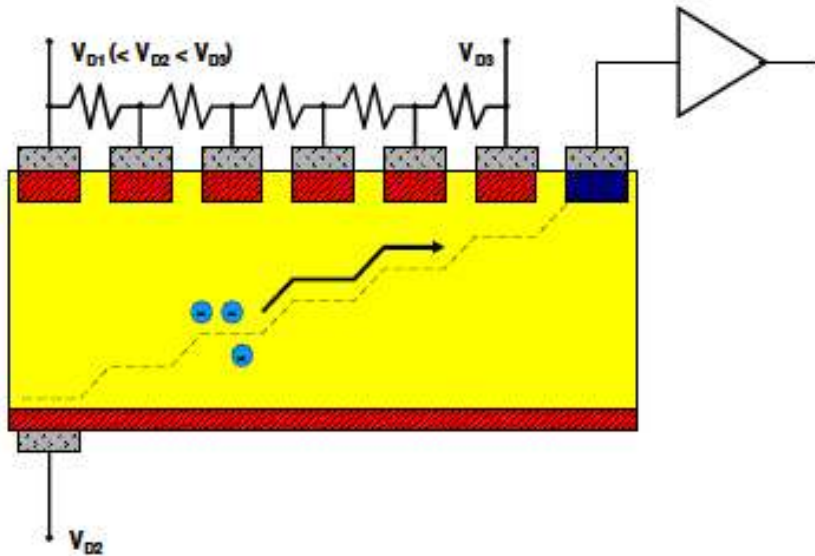
- holes move to the p+ electrodes
- electrons assemble in the center of the wafer
- uncontrolled charge diffusion to the anode

Apply horizontal electric field, to drift electrons to the anode

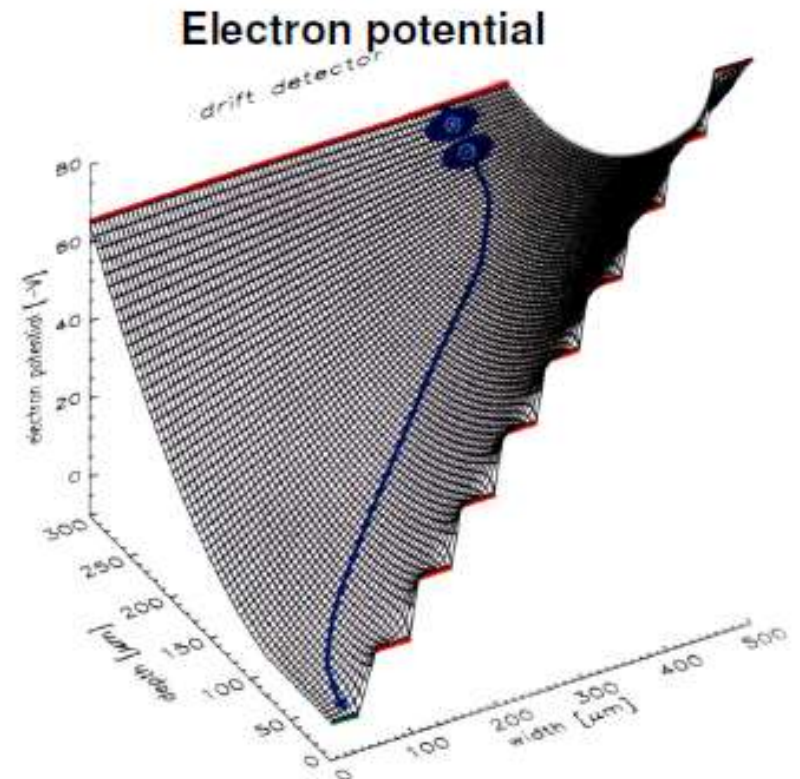
Function of Silicon Drift Detector



Full depletion of the bulk under reverse bias

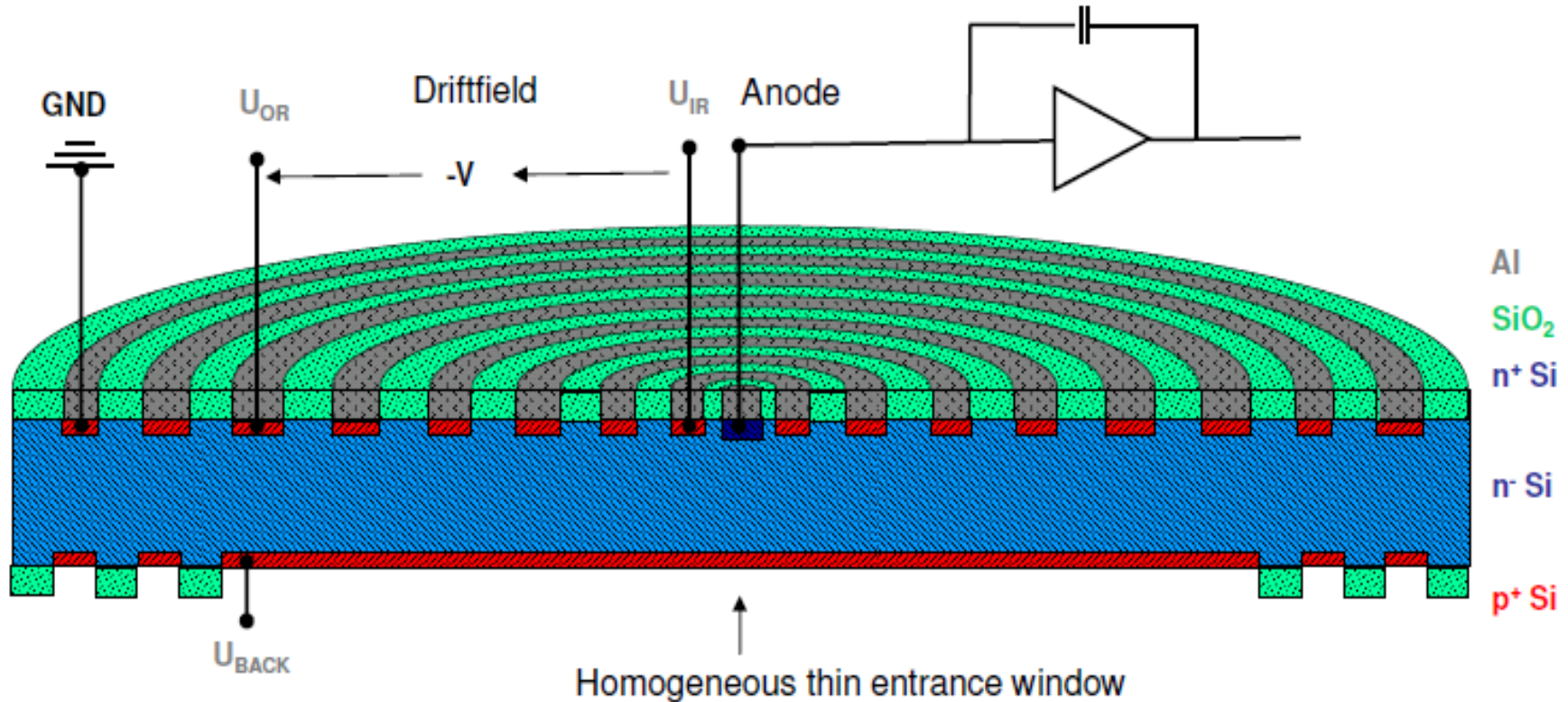


- Homogeneous entrance window
uniform sensitivity for x-rays
- Drift electrodes only at one side
simpler technology
- Sloped potential valley



Position measurement possible by hole signals from structured rear side

Silicon Drift Detector with Circular Geometry



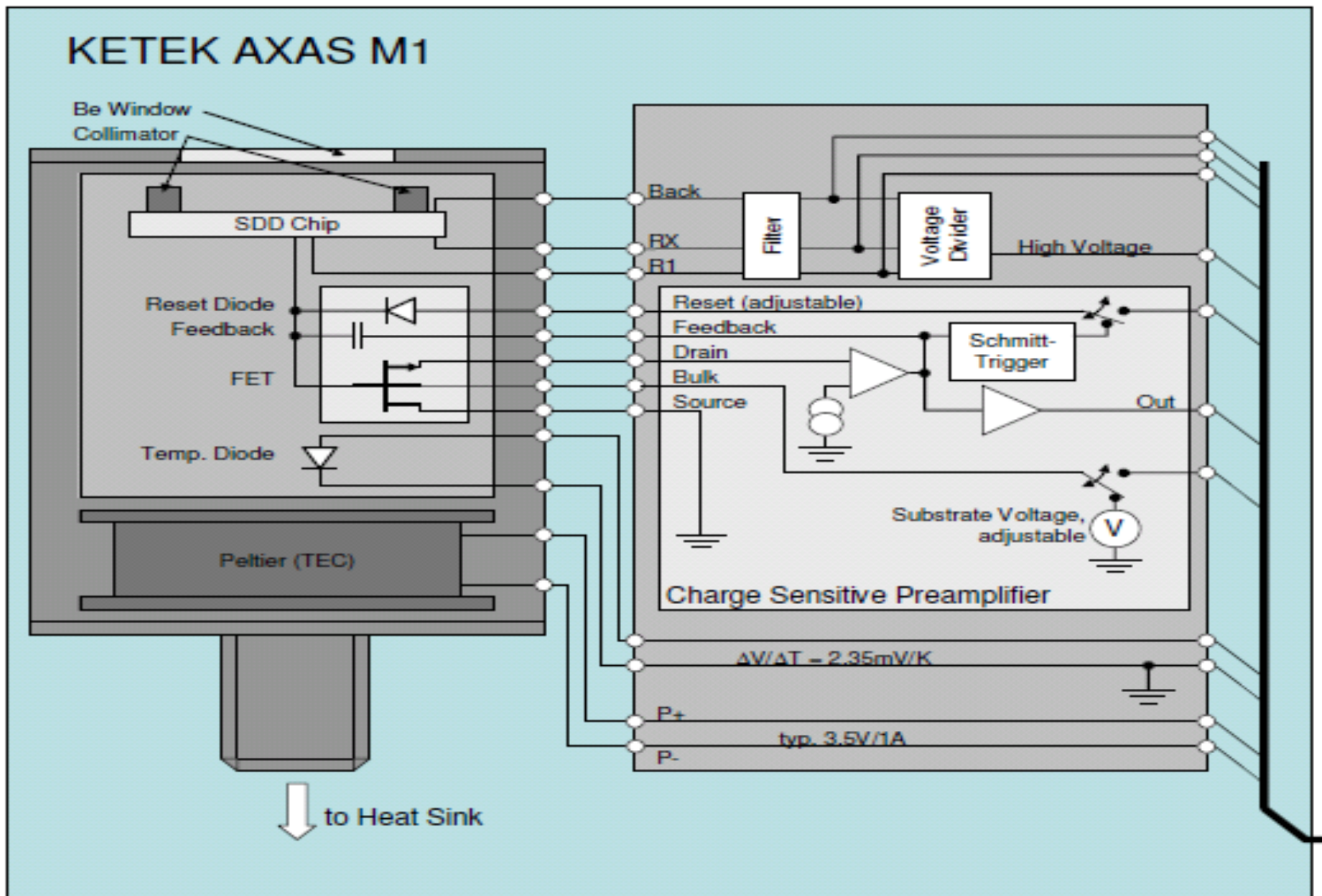
Small size of output capacitance

- high energy resolution
- high count rate capability

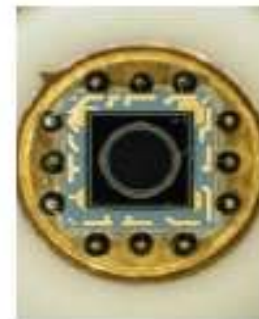
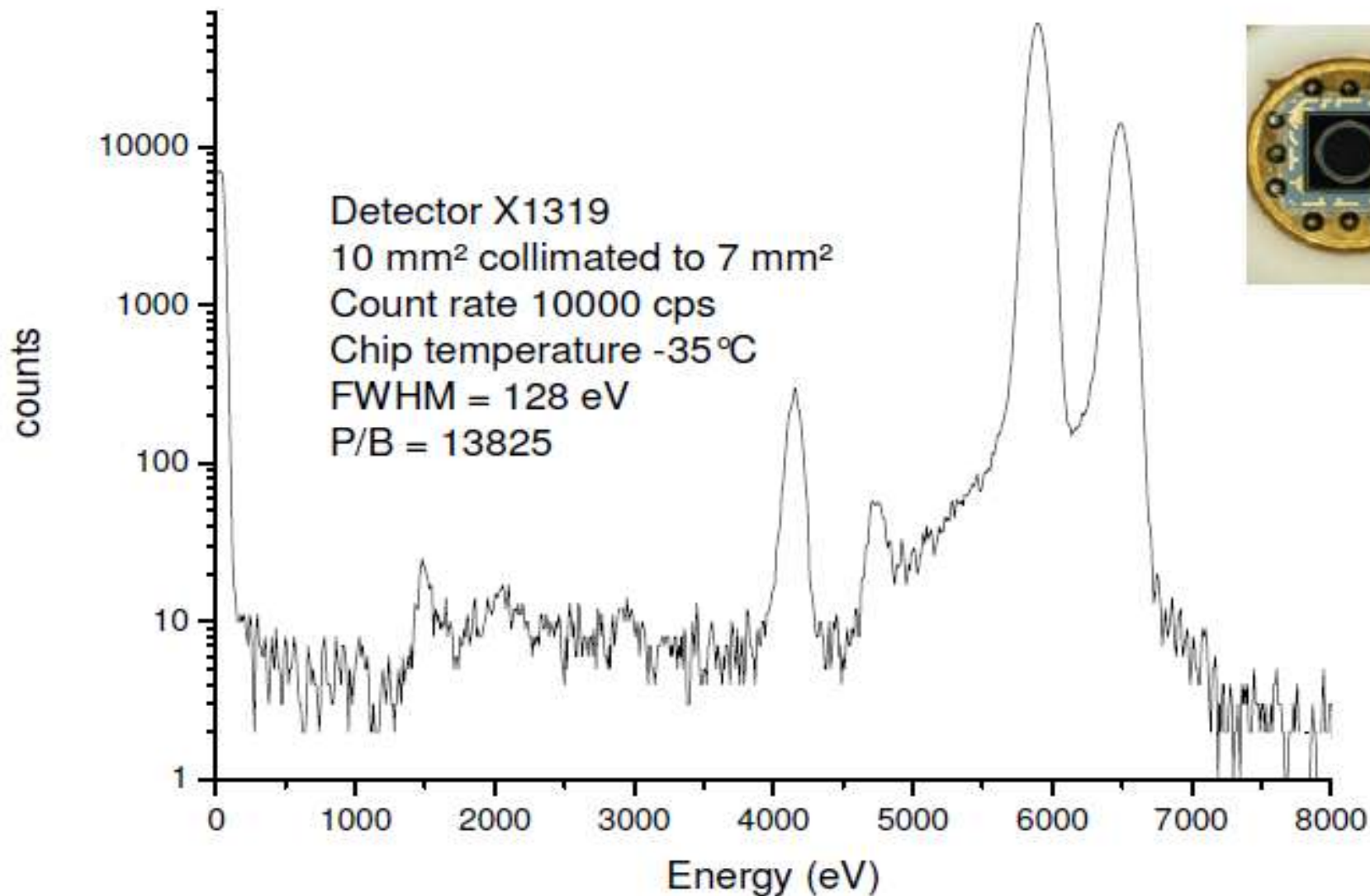
Low leakage current level

- operation at moderate cooling
- no liquid nitrogen necessary

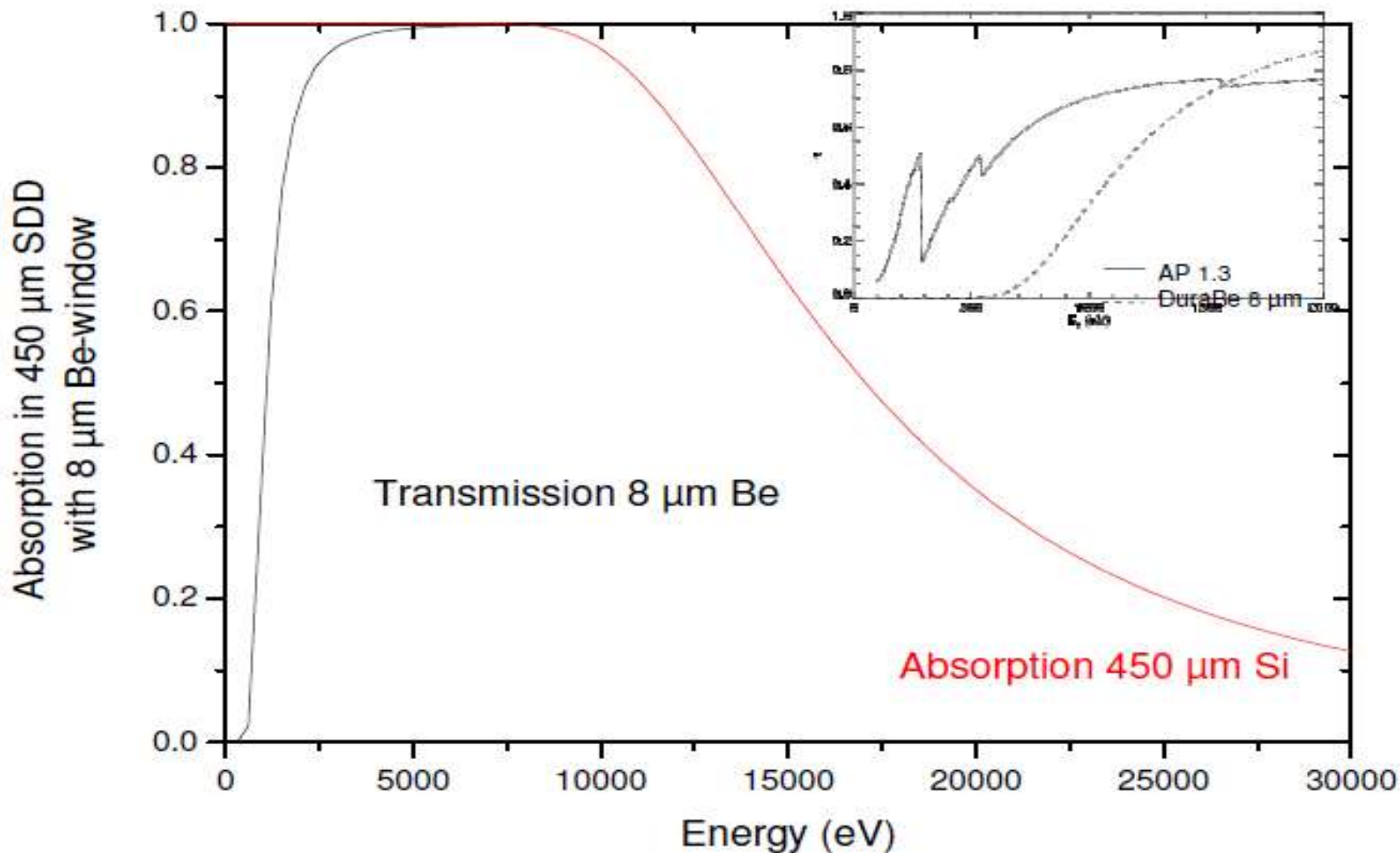
General Requirements of SDD Electronics



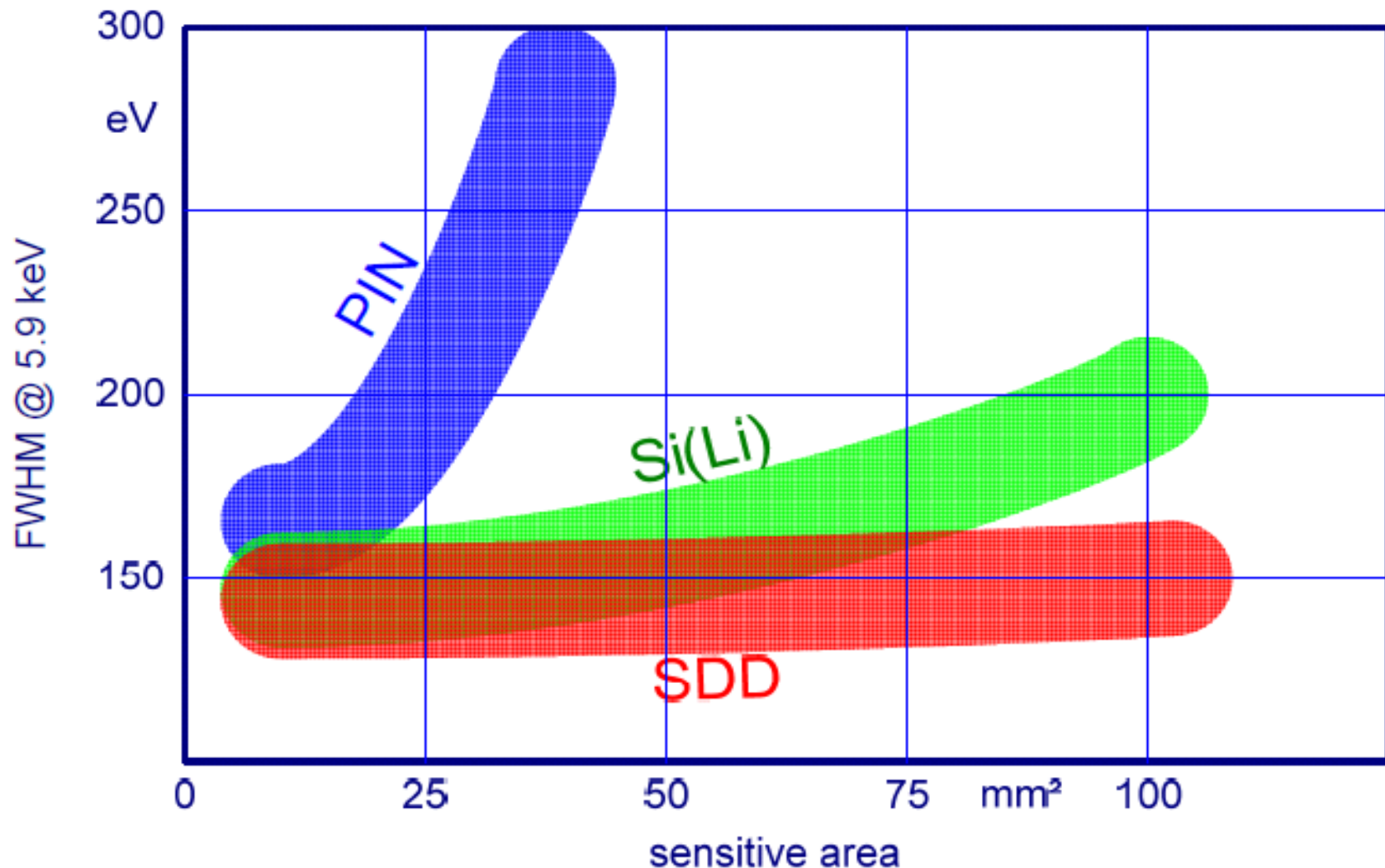
Spectrum of 10 mm² KETEK Vitus SDD



Absorption curve for 450 μ m SDDs



Large Area Silicon Detectors



Depletion layer thickness w :

$$w \text{ (cm)} = 0.5 \times 10^{-4} (\rho U)^{1/2}$$

ρ (Ωcm)	resistivity
U (V)	bias voltage

Capacitance C :

$$C \text{ (pF)} = 2 \times 10^{-4} A (\rho U)^{-1/2}$$

A (cm^2)	junction area
-----------------------	---------------

Reverse current i_R :

$$i_R \text{ (A)} = i_D + i_S + i_G$$

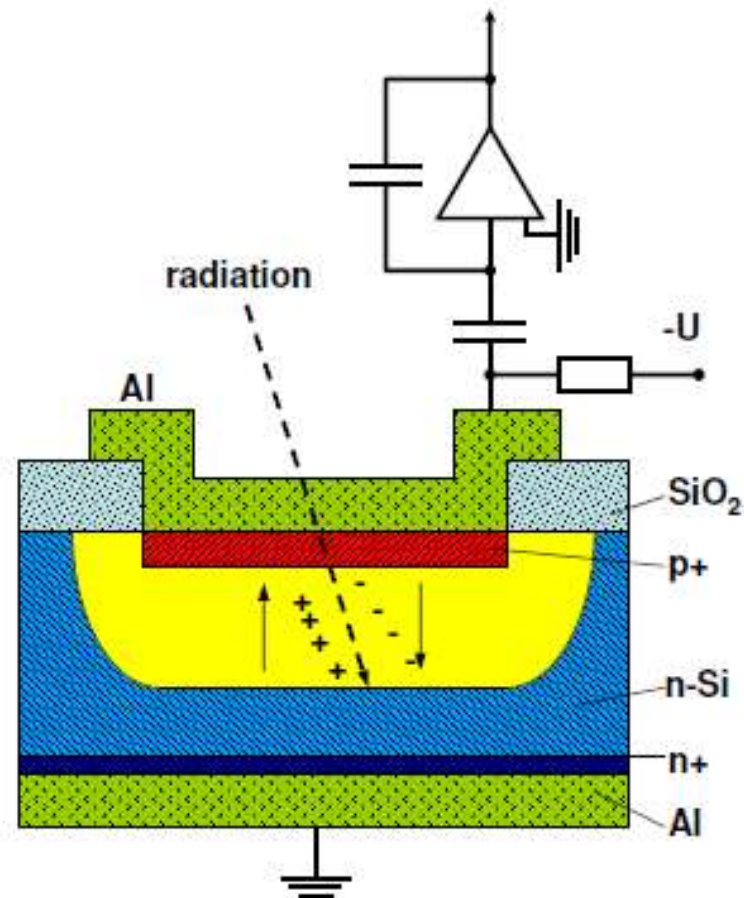
i_D diffusion current
 i_S surface leakage c.
 i_G generation current

For deep depletion layer :

$$i_R = i_G = q g V = q (n_i/\tau) A 0.5 \times 10^{-4} (\rho U)^{1/2}$$

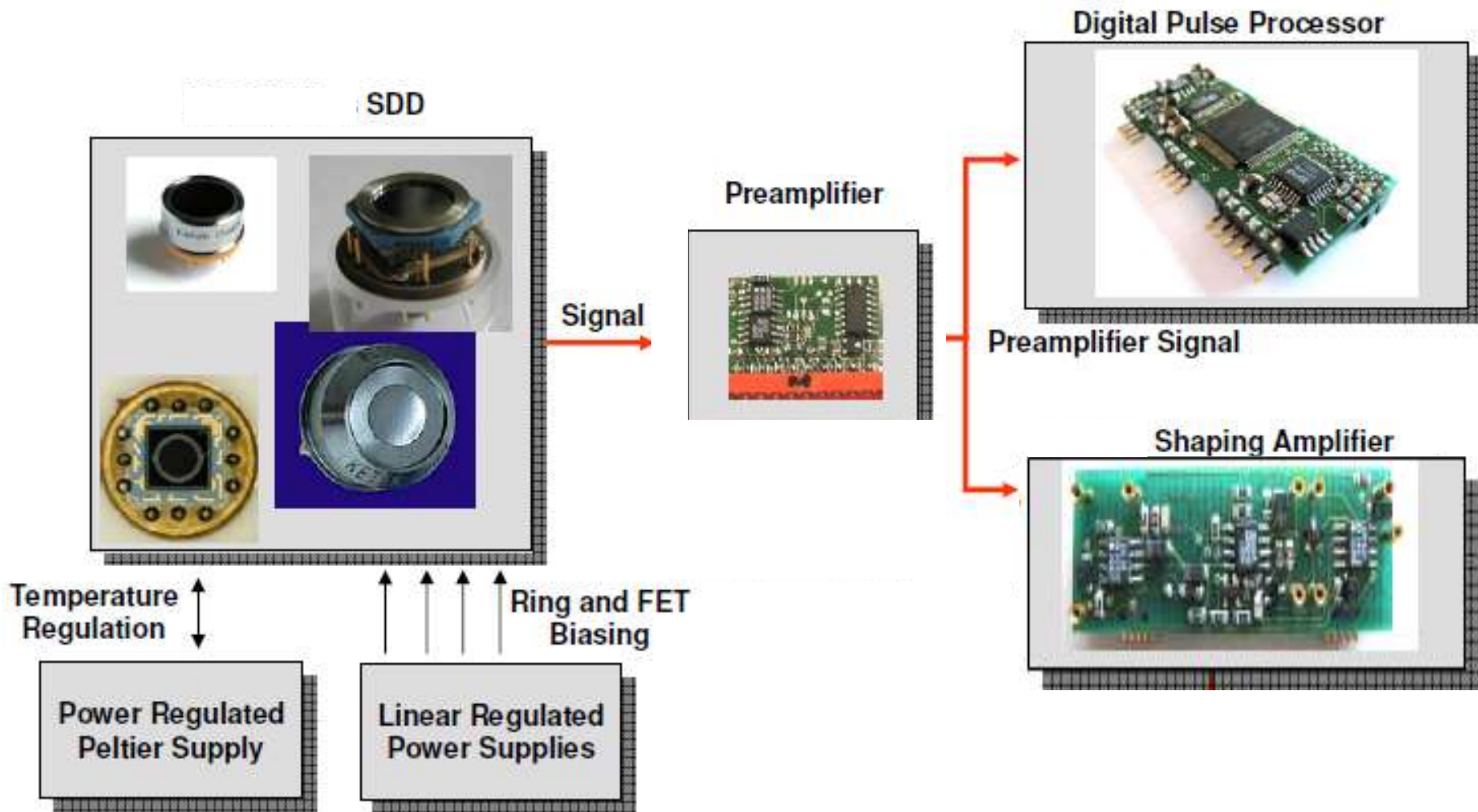
$$i_R \sim U^{1/2}/\tau$$

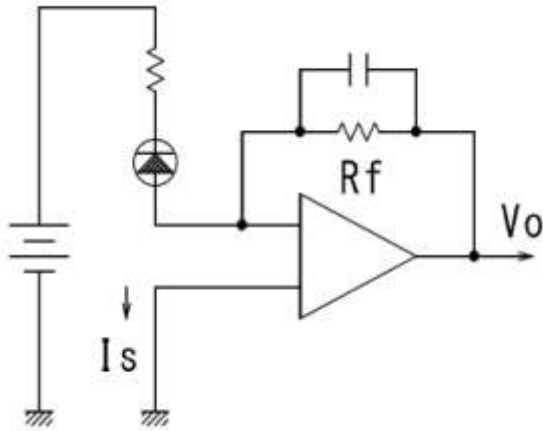
n_i	$1.45 \times 10^{10} \text{ cm}^{-3}$
	intrinsic carrier cor
τ	lifetime
q	$1.6 \times 10^{-19} \text{ A s}$



Noise sources:

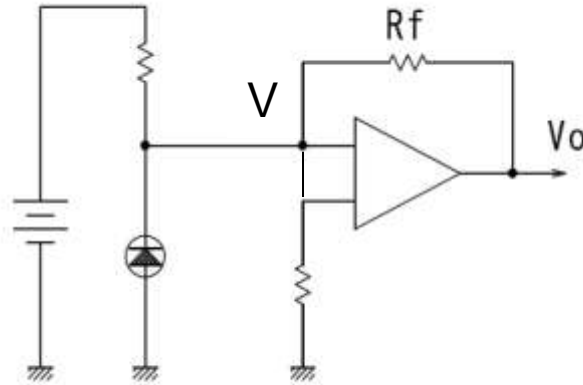
- capacitance
- reverse current





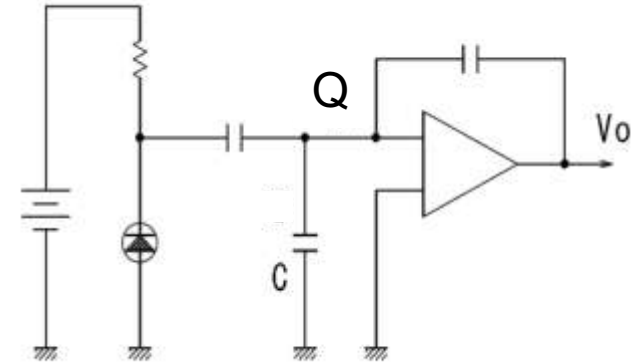
$$V_o = R_f \cdot I_s$$

a) current sensitive



$$V_o = \left(\frac{R + R_f}{R} \right) V$$

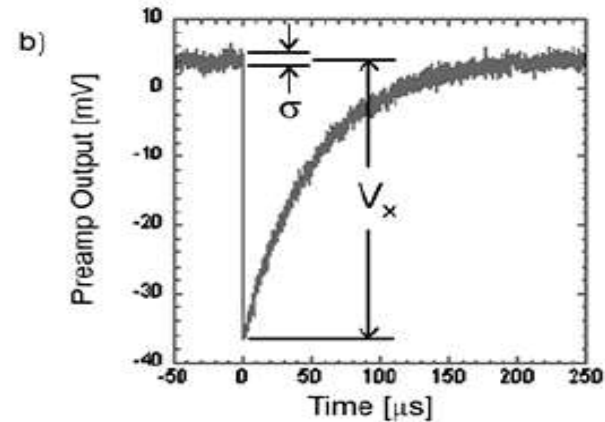
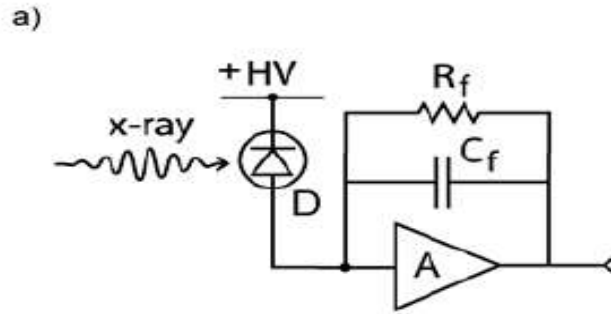
b) V0 leakage sensitive



$$V_o = \frac{Q}{C}$$

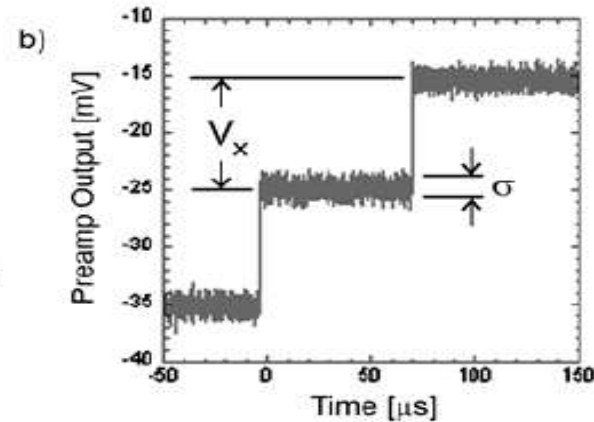
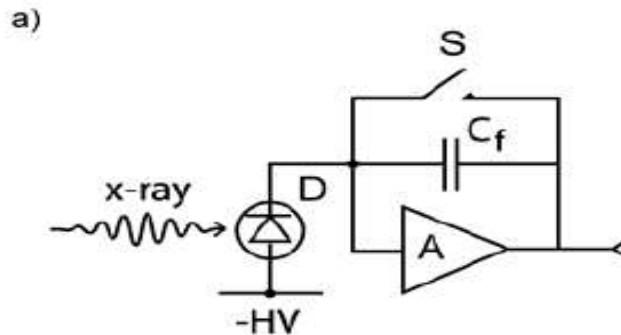
c) Charge sensitive

RC type



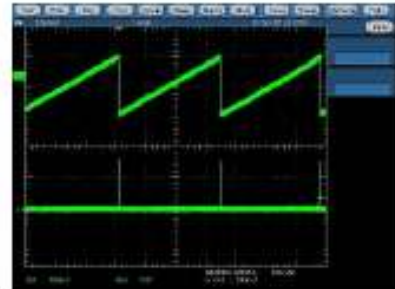
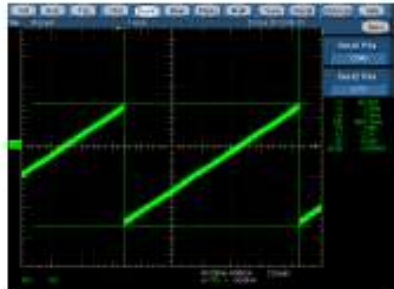
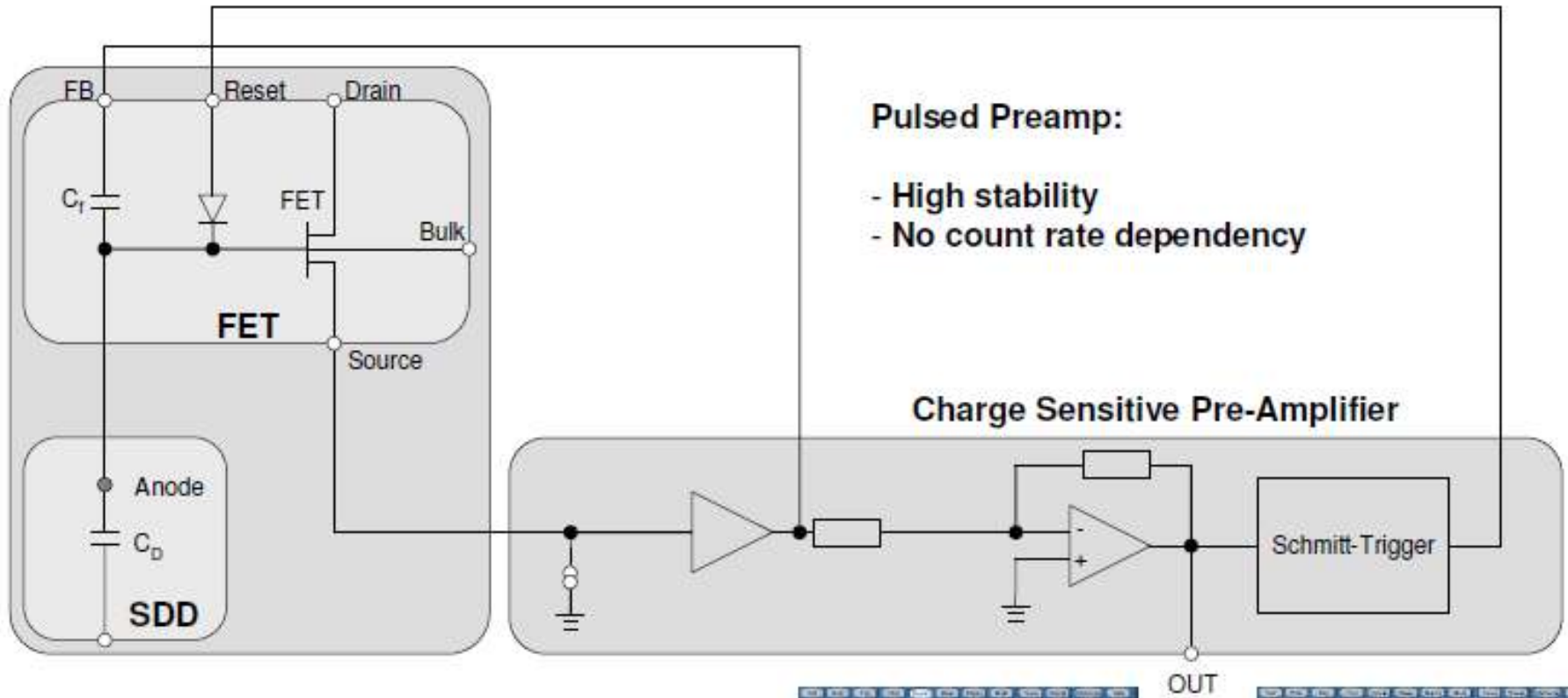
- a) RC-type charge sensitive preamplifier with a positively biased detector;
 b) Output on absorption of an x-ray. Note that the step has a falling edge, thus the signal polarity is negative.

Reset type

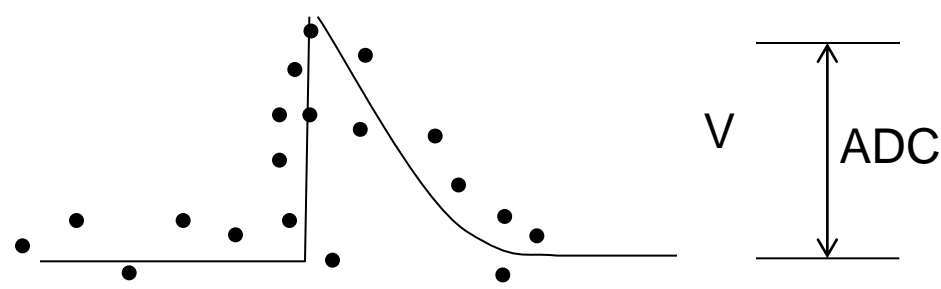
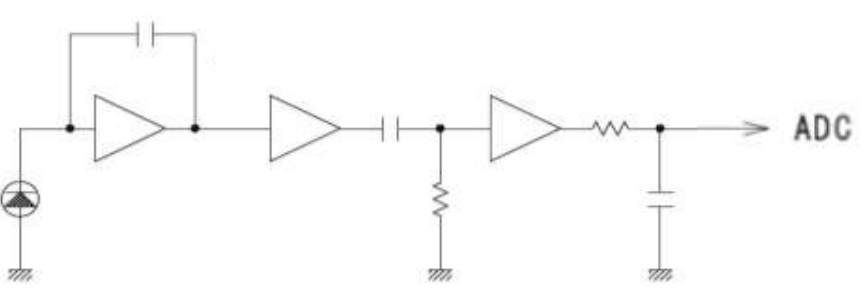
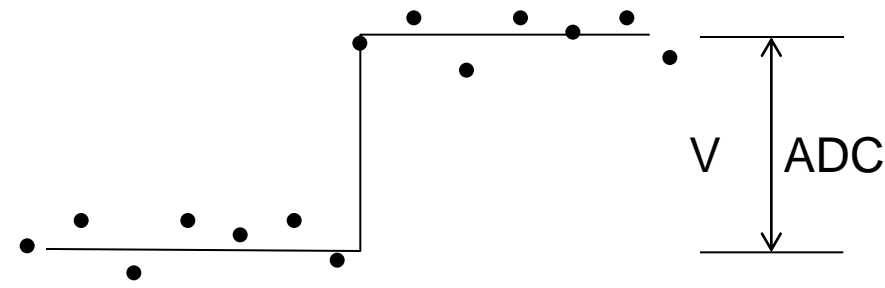
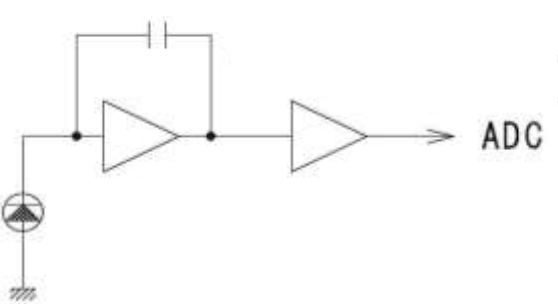
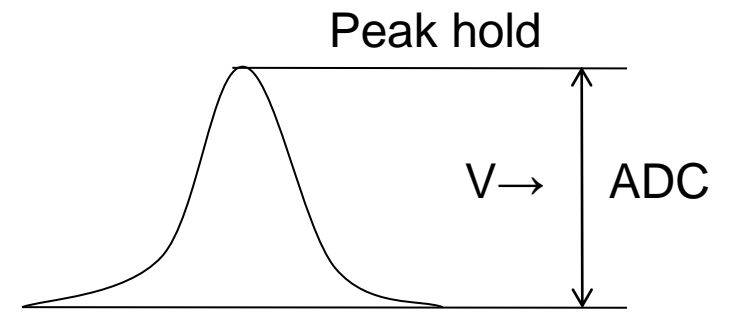
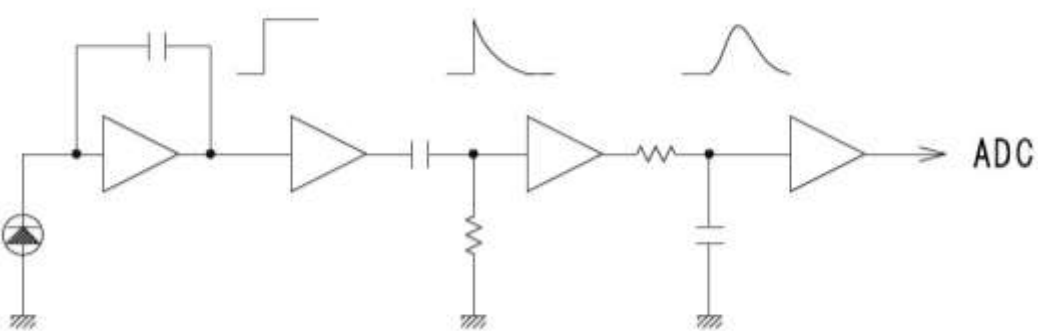


- a) Reset-type charge sensitive preamplifier with a negatively biased detector;
 b) Output on absorption of x-ray rays. Note that the steps have a rising edge, so that the signal polarity is positive.

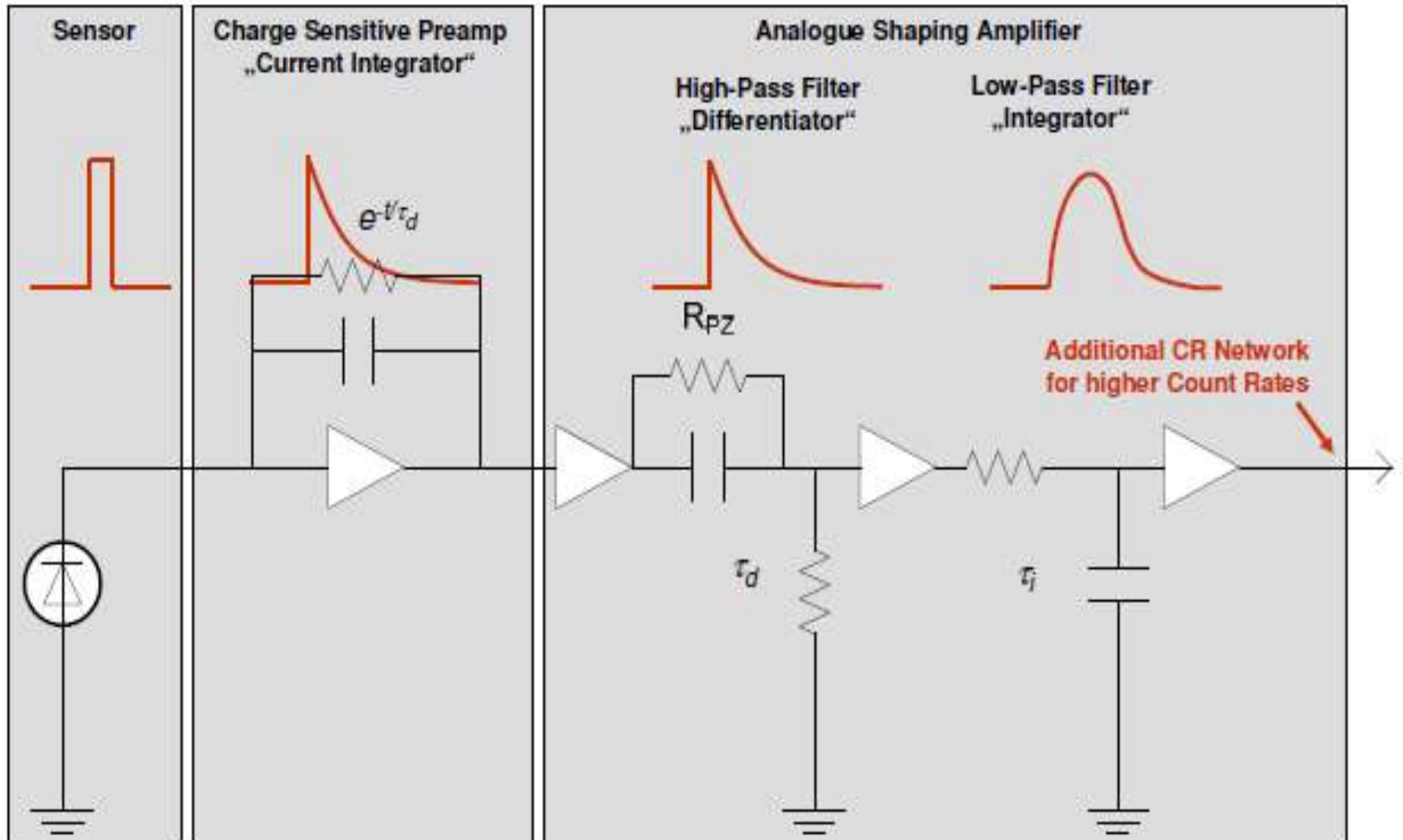
Reset type Preampfilter

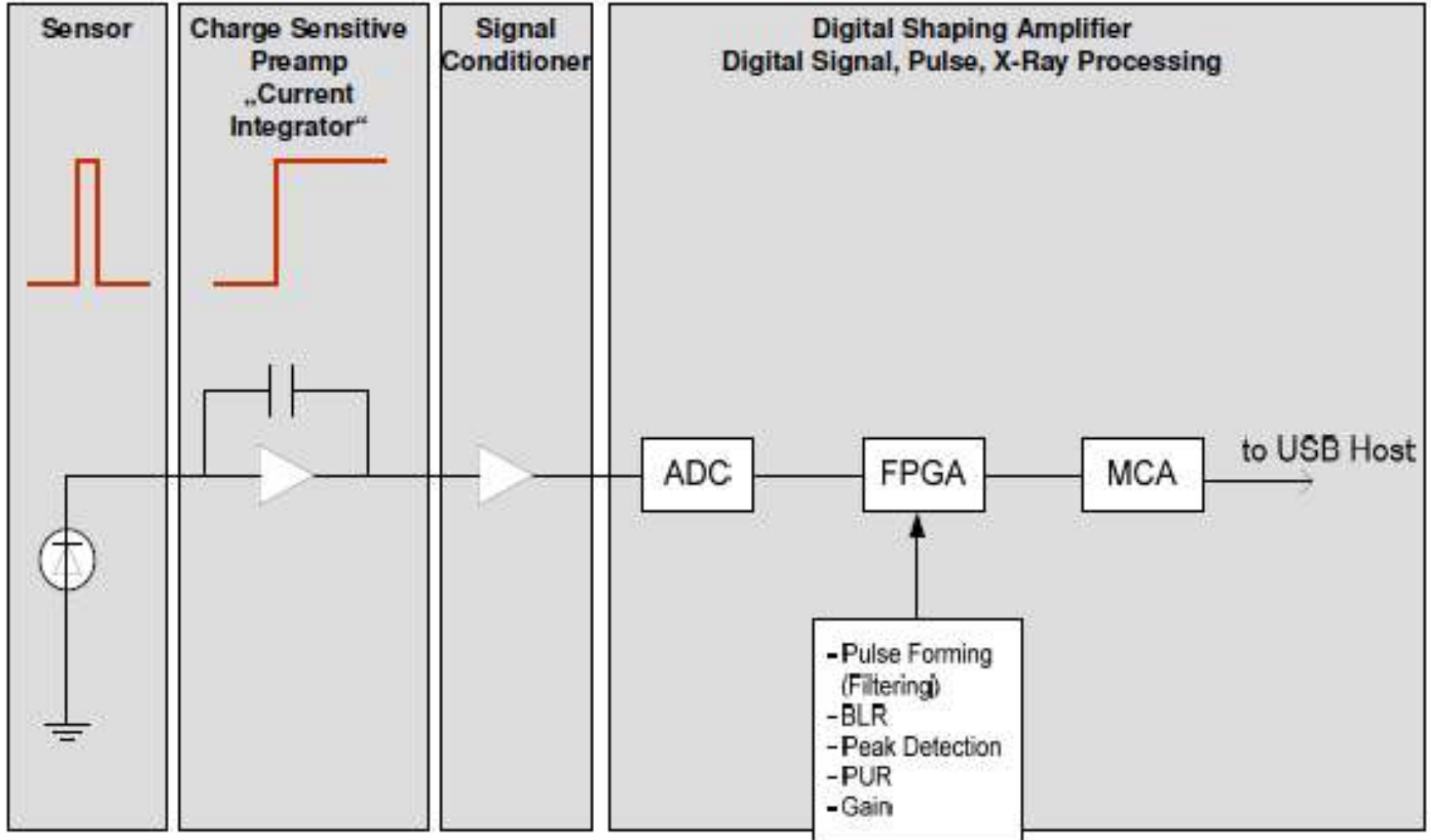


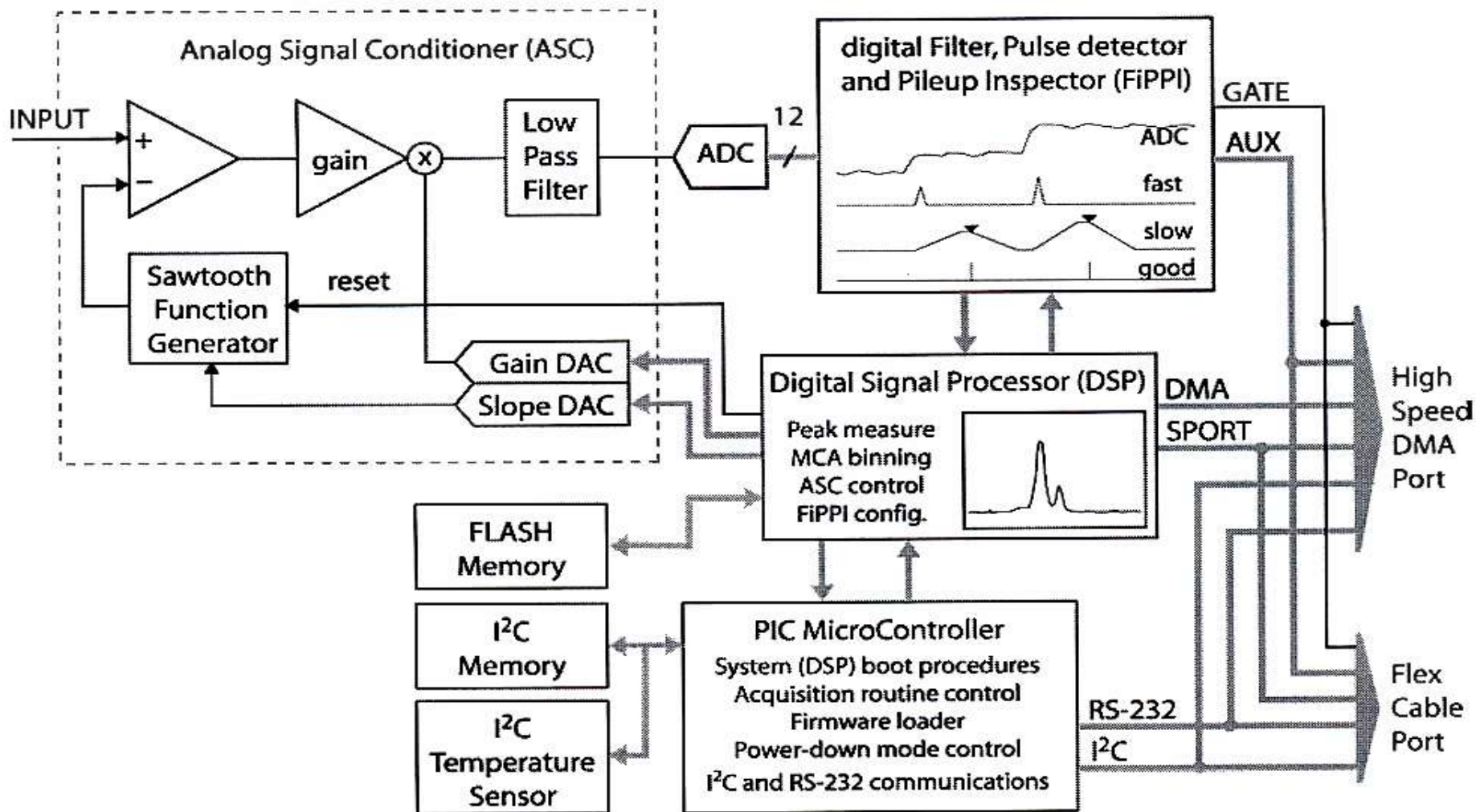
OUT

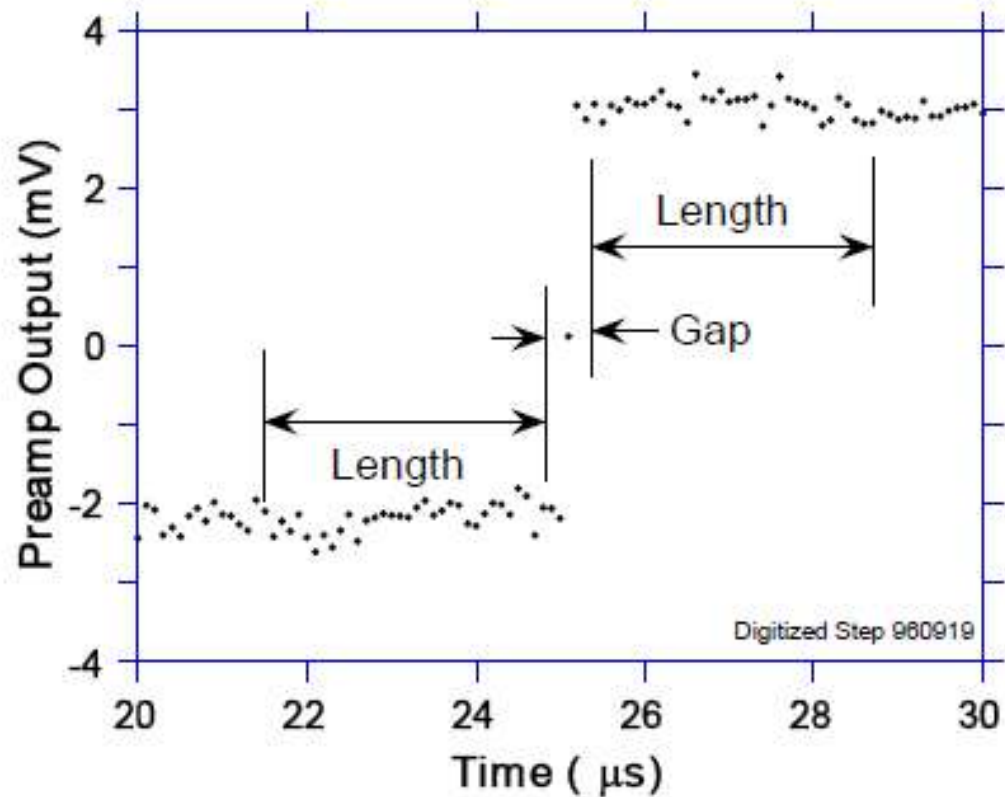
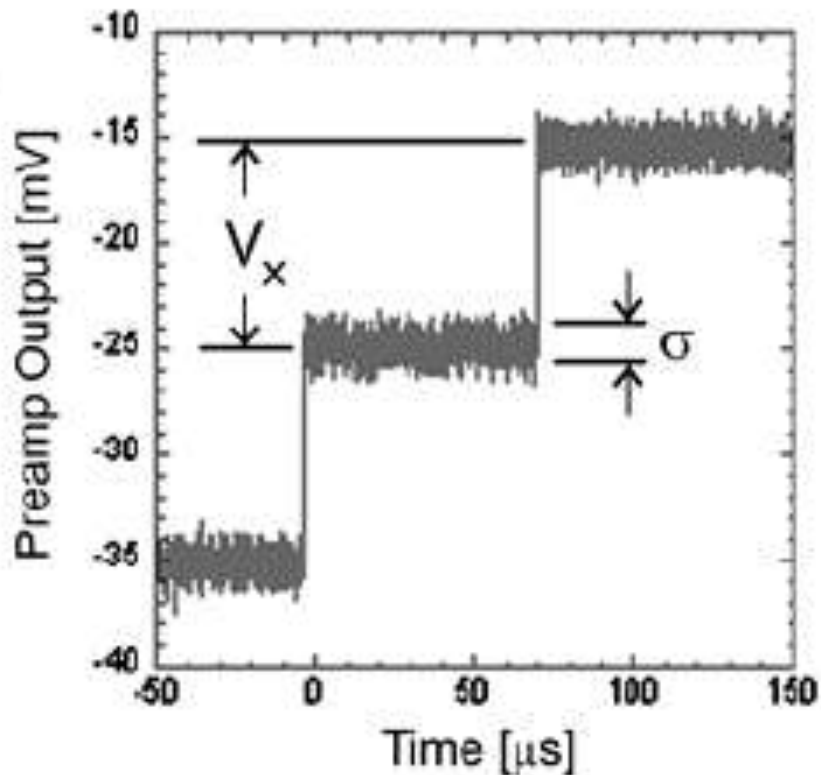


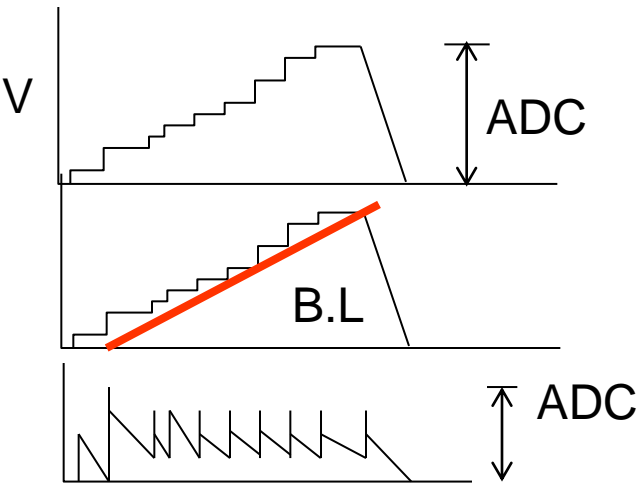
Principle of Analogue Signal Shaping











XIA

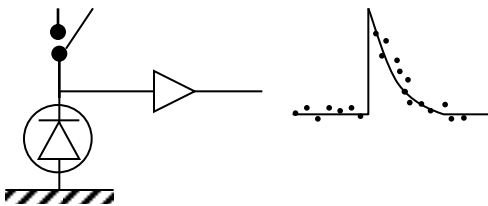
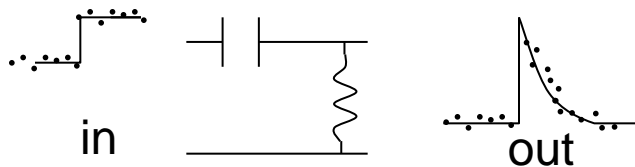
Analog Signal Conditioner (ASC):

- Subtraction of a Saw Tooth Function from the ramped Preamplifier Output Signal
- Amplification and Offset of the Difference Signal to fit the ADC input range

KETEK

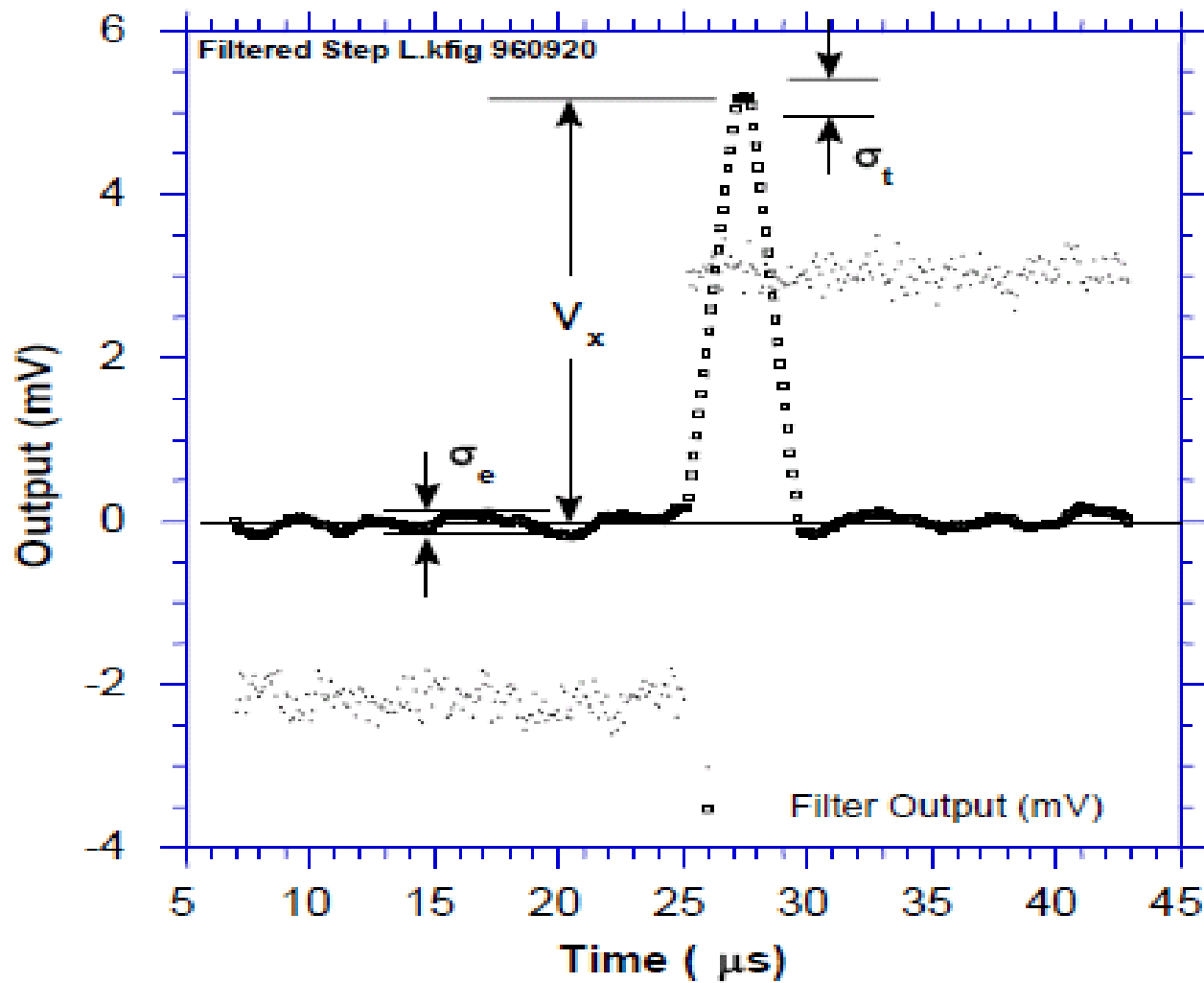
Analog Signal Conversion

- Conversion of the ramped Preamplifier Output Signal to an exponential Output Signal by differentiating with a High Pass Filter of maximum 6 μ s Decay Time
- Amplification and Offset of the differentiated Signal to fit the ADC input range

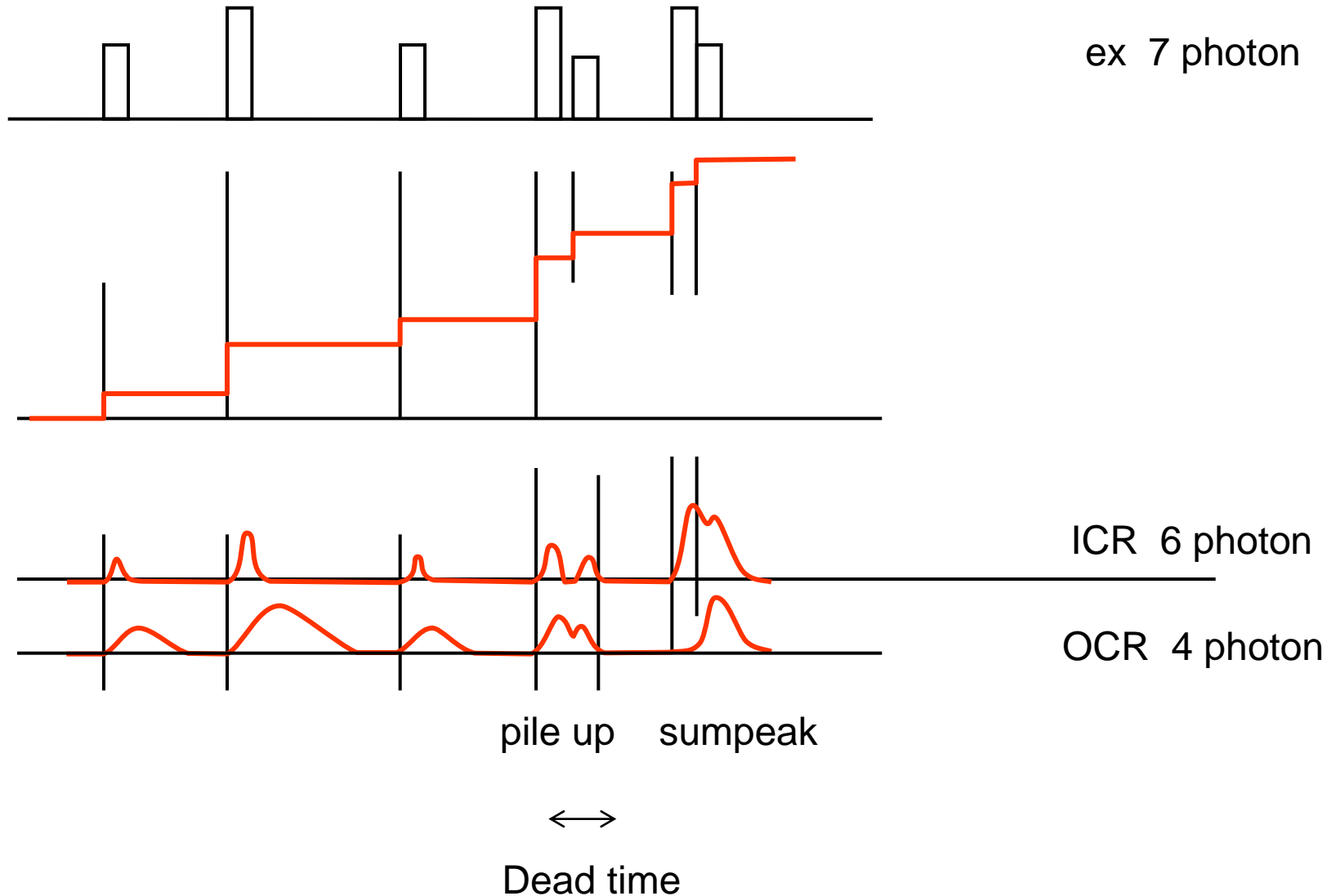


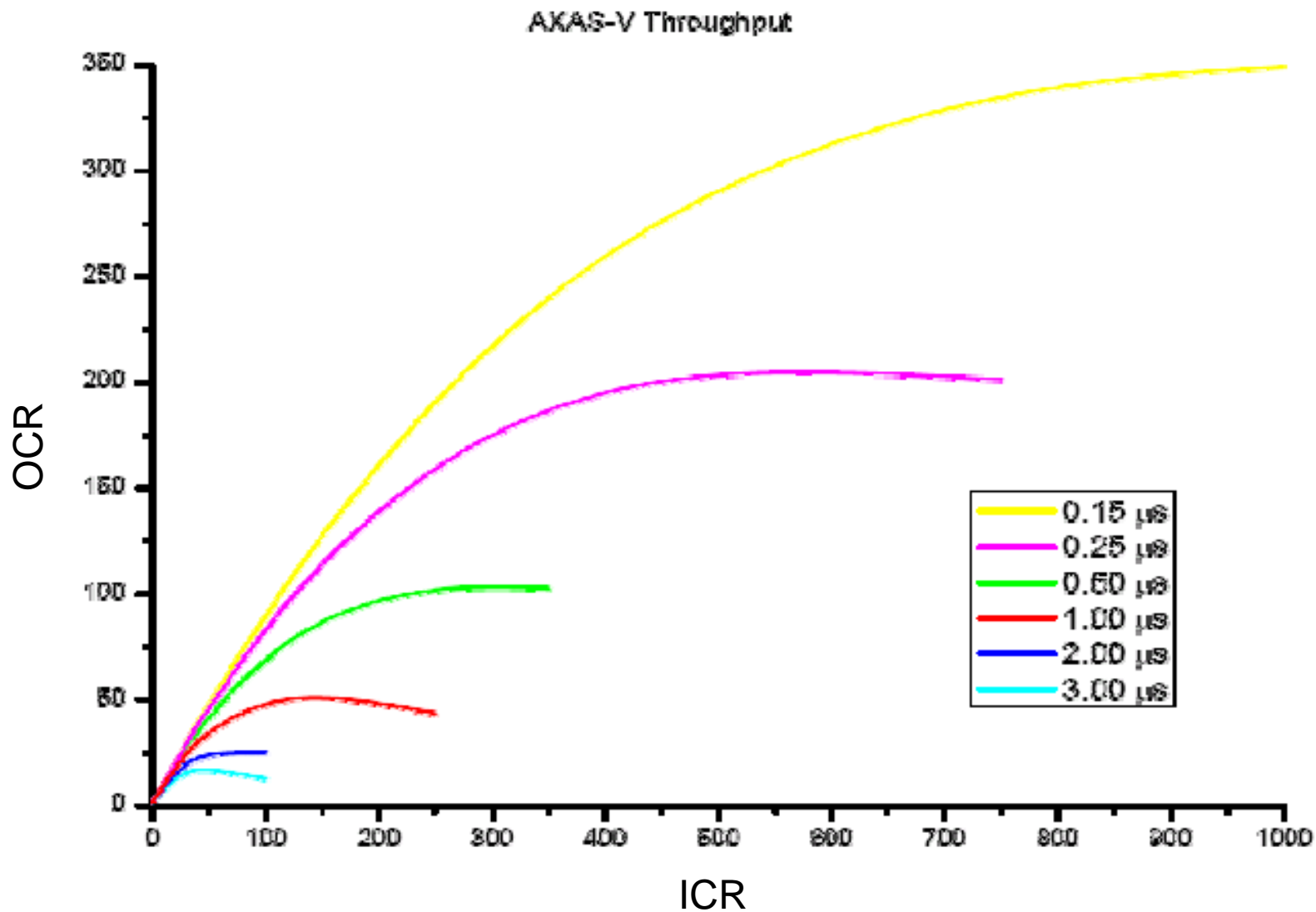
Oxford Instruments

High Frequency Reset triggered by the DSP to keep the ramped Preamplifier Output Signal in the ADC input range



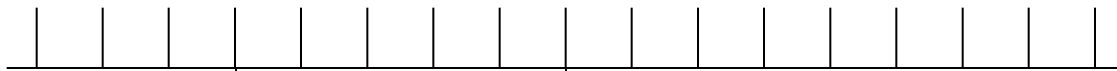
Displayed over a longer time period to show baseline noise.



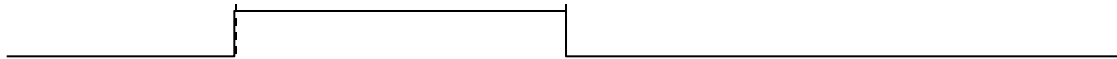


True time & Live time

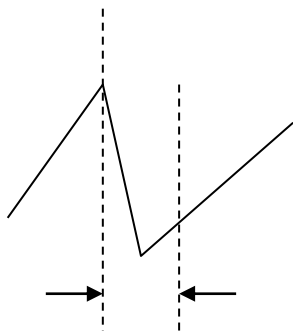
true time



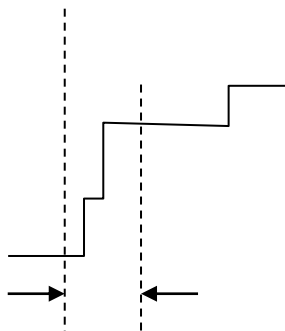
ADCB



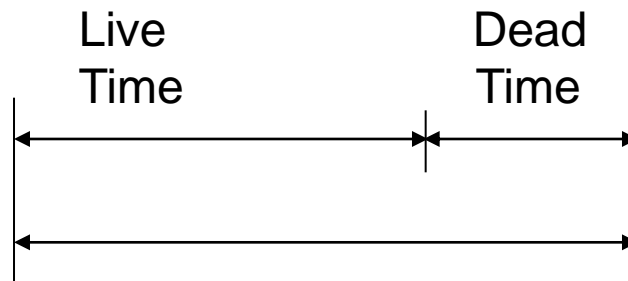
live time



inhibit

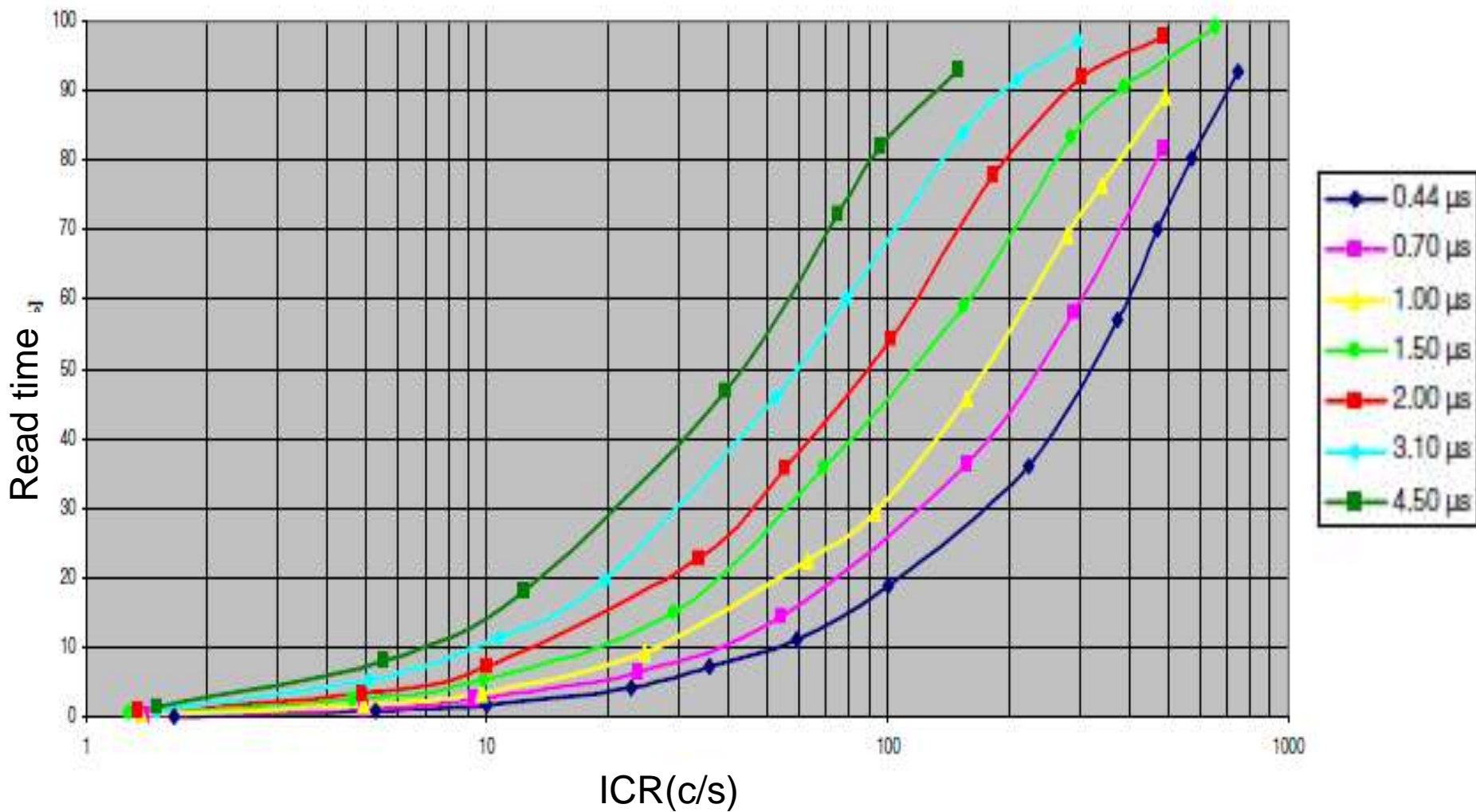


pile up

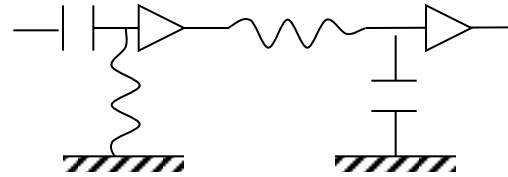


True Time

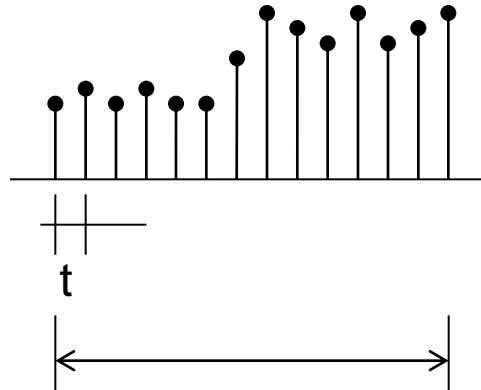
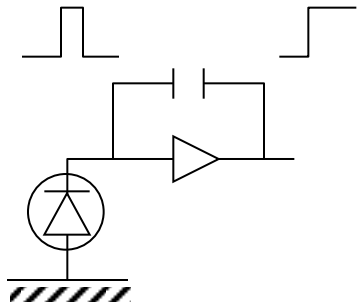
Dead Time versus Input Count Rate



Shaping time & Peaking time



t_s = Shaping time
= Time constant
for Filter

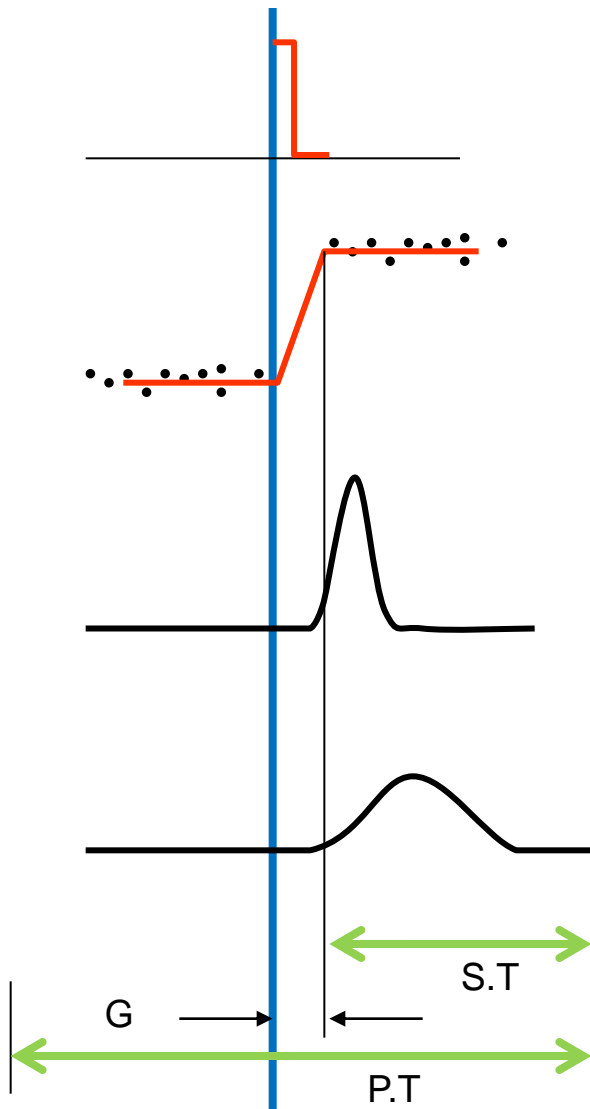


$t_p = t \times n$
 t = time of sampling
 n = number of sampling

for ex. 16MHz $t = 62.5\text{nsec}$
 $n = 24$
 $t \times n = 62.5 \text{ nsec} \times 24 = 1.5\mu\text{sec}$

t_p = Peaking time

Relation between Shaping time & Peaking time



photon coming to detector

charge increase at preamplifier

short shaping time

long shaping time

$$P.T > 2 \times S.T$$

Noise Sources of a SDD

Serial Noise

- Determined by capacitance of complete setup: anode capacitance + input capacitance of FET + stray capacitance (bond wire + mounting technique)
- Dependent on transconductance of the FET
- Slightly temperature dependent

Influences short shaping times (high count rates applications)
reducing serial noise → high count rates with very good FWHM

1/f Noise

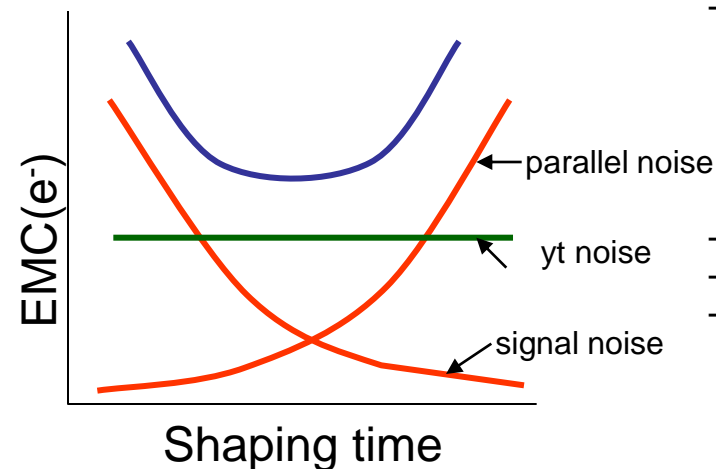
- Dependent on mounting technique
- Noise of FET
- Dependent on capacitance

Independent of shaping time;
reducing the 1/f noise improves the energy resolution for all shaping times

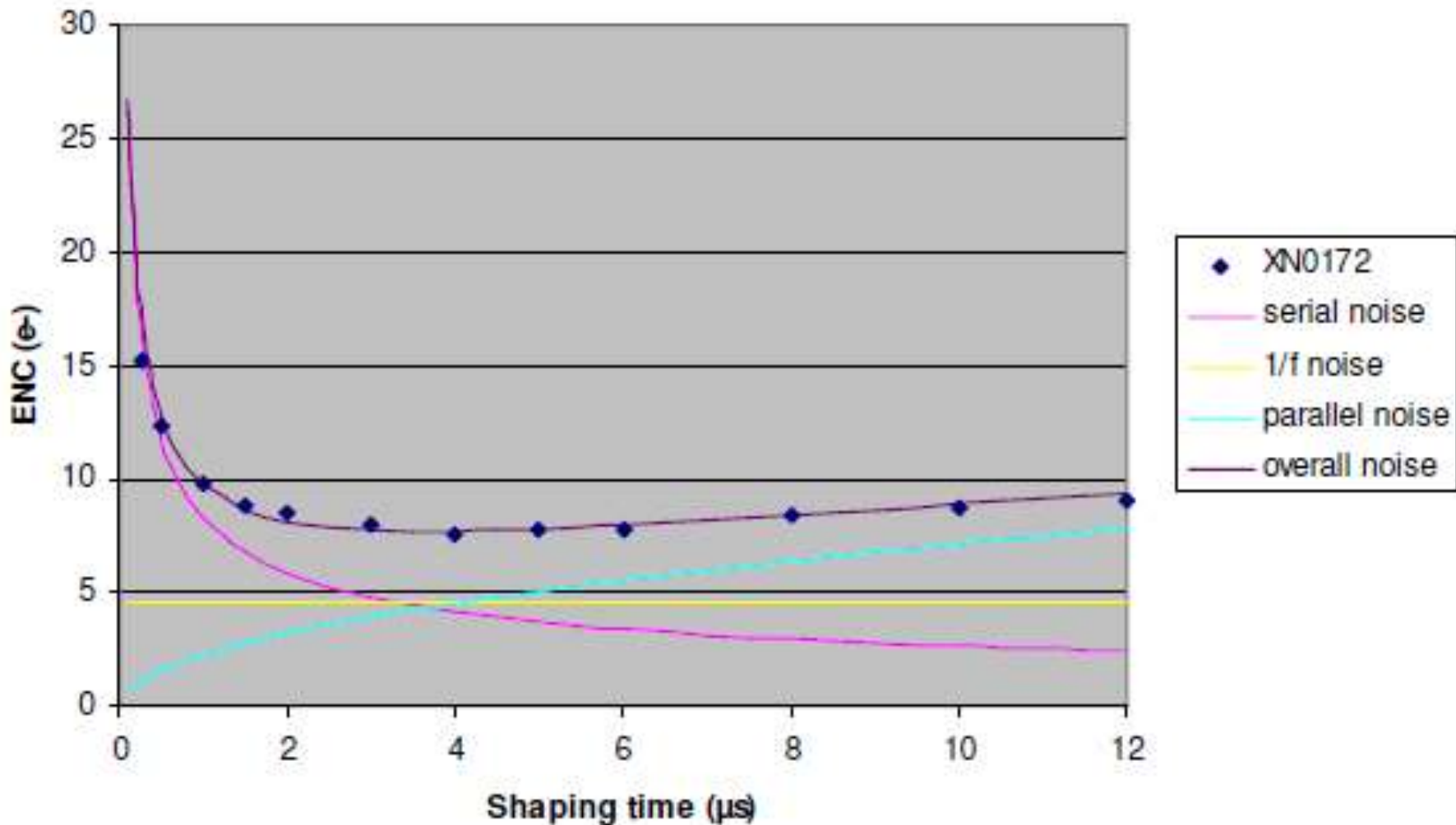
Parallel Noise

- Dependent on leakage current of SDD (therefore strong dependency on operating temperature – cooling by approx. 7° C halves leakage current)

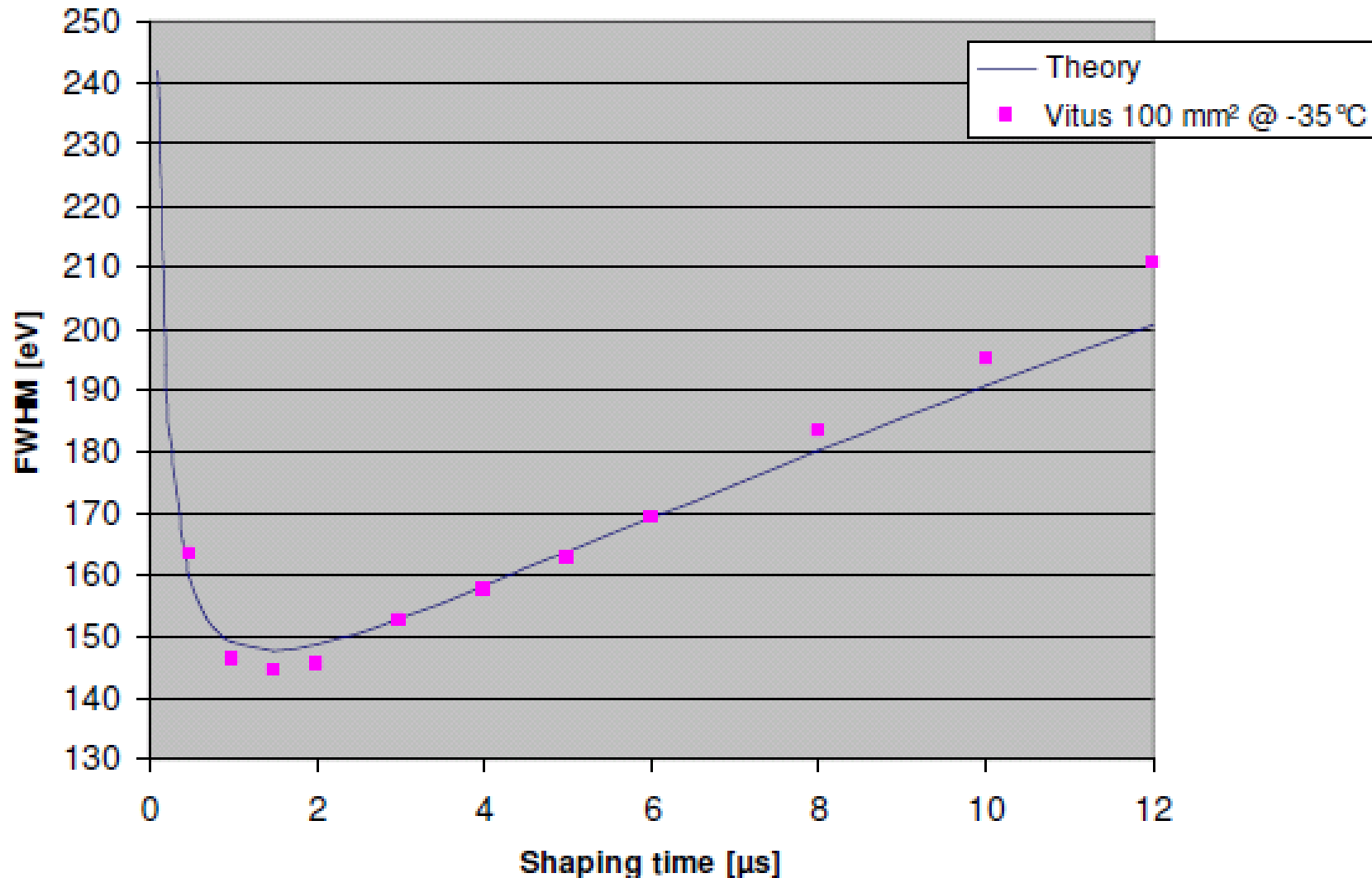
Influences long shaping times; can be reduced by lower operating temperatures
Reducing parallel noise is important for large area detectors and for operating conditions under high ambient temperatures



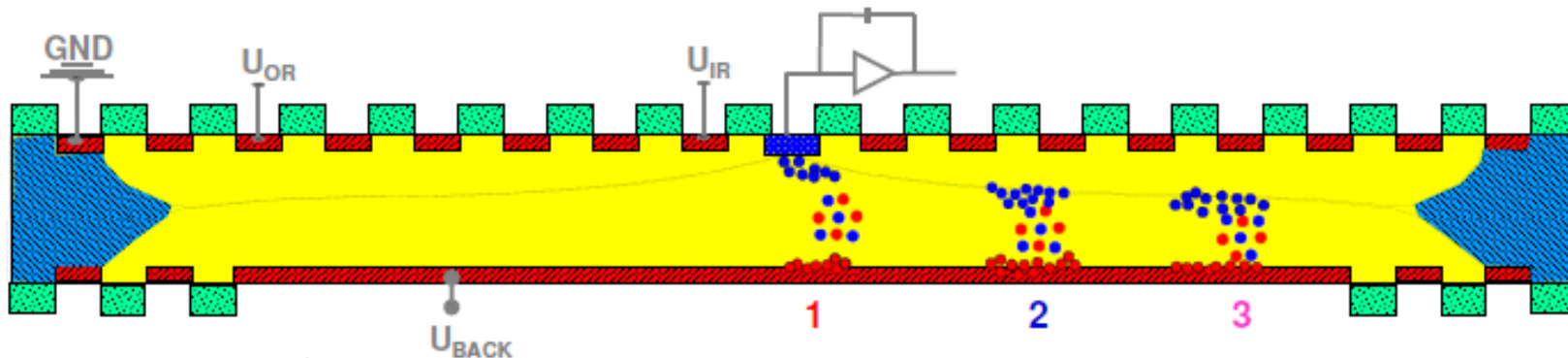
Noise plot of a 10 mm² Vitus SDD



Noise plot of a 100 mm² Vitus SDD



Function of Silicon Drift Detector

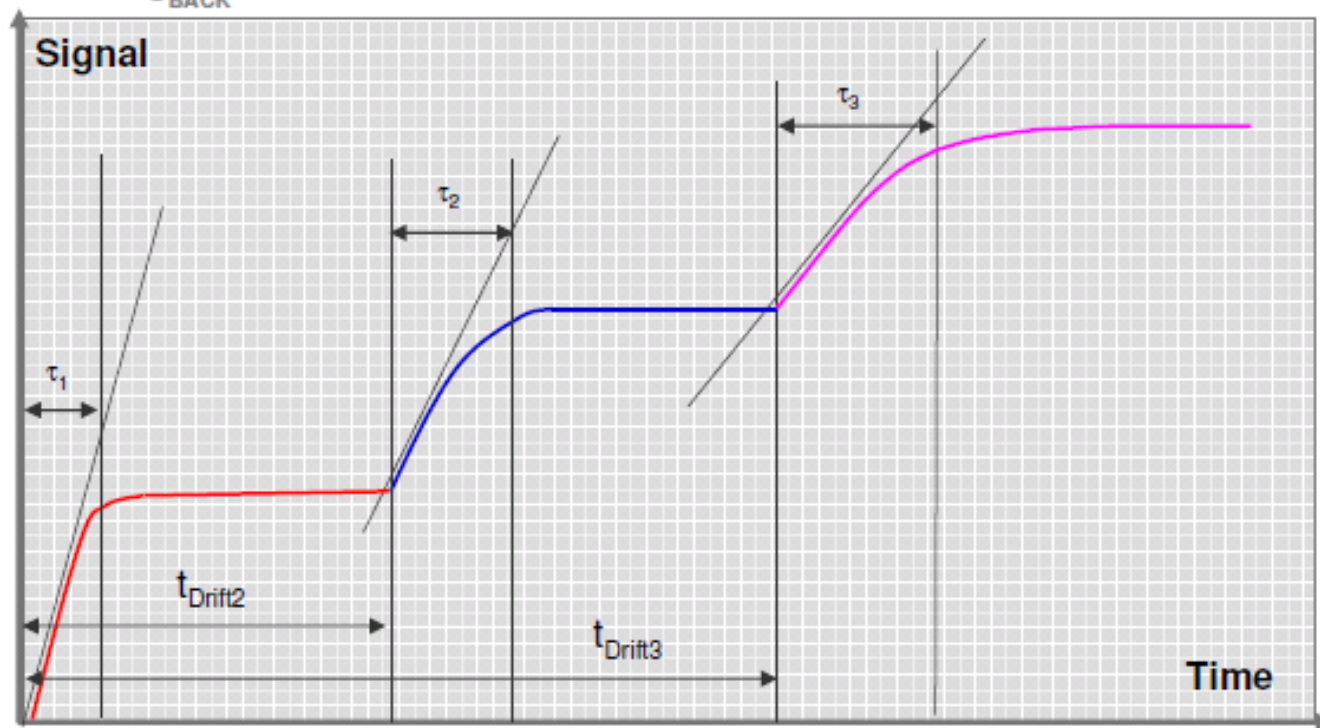


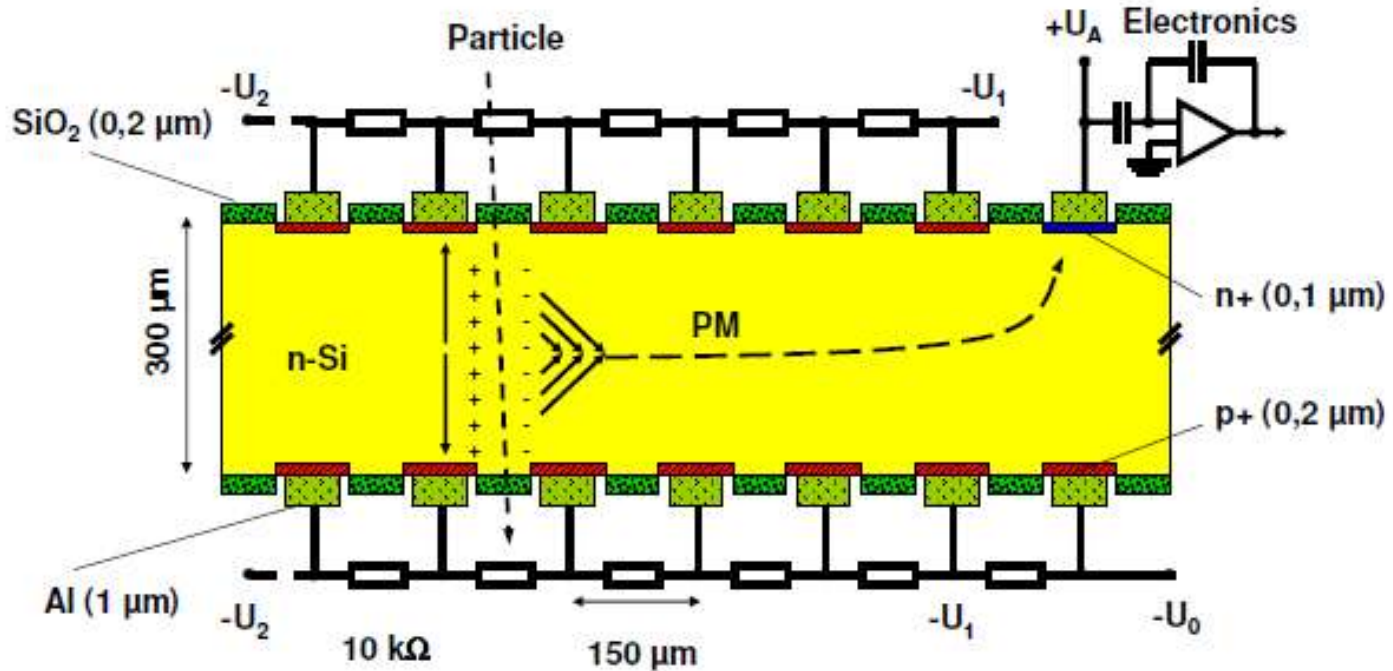
Charge Collection:

Event 1 **signal 1**

Event 2 **signal 2**

Event 3 **signal 3**





Horizontal electric field by

- division of electrodes into strips
- applying of increasing bias at strips

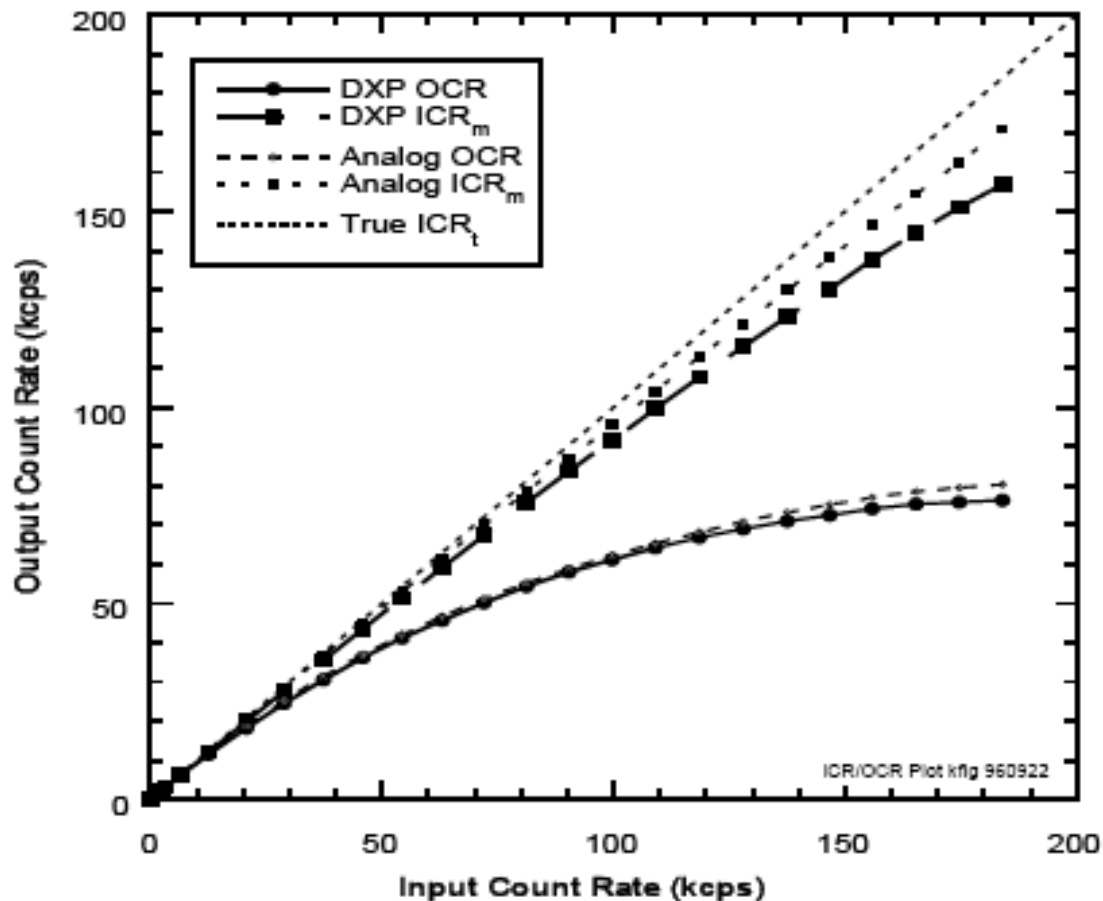
Charge collection

- electrons are drifting to readout anode
- low noise amplification of signal at anode

signal height \Rightarrow energy of radiation
drift time \Rightarrow position of radiation

Comparison of Analog & Digital

NOTE: The DXP's peaking time is twice as long as the analog system peaking time in this comparison, and yet the throughput is nearly the same.



Curves of ICR_m and OCR for the DXP using 2 μs peaking time, compared to a common analog SCA system using 1 μs peaking time.

Thank you for you attention

テクノエックス

検索



<http://techno-x.co.jp/>